ATG-1200 Y3

TRANSPONDER and DME TEST SET

OPERATION and MAINTENANCE MANUAL



10200 WEST YORK STREET/WICHITA, KANSAS 67215 U.S.A. /(316) 522-4981/TWX 910-741-6952

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Manual Part Number: 1002-1456-900

ATC-1200Y3

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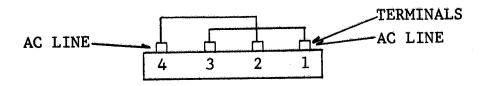
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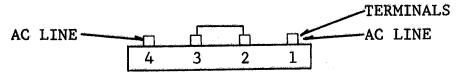
ATC-1200Y3 NOTICE

FOR 115 VAC INPUT OPERATION CONNECT POWER TRANSFORMER LEADS AS FOLLOWS:

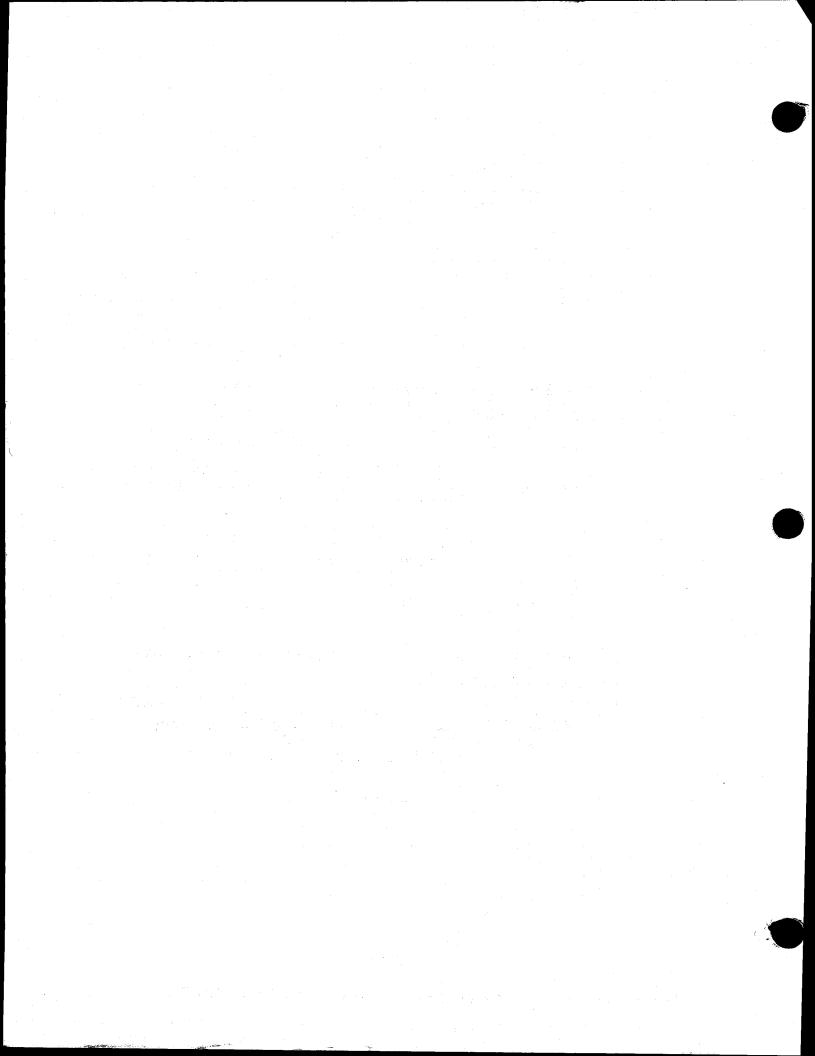


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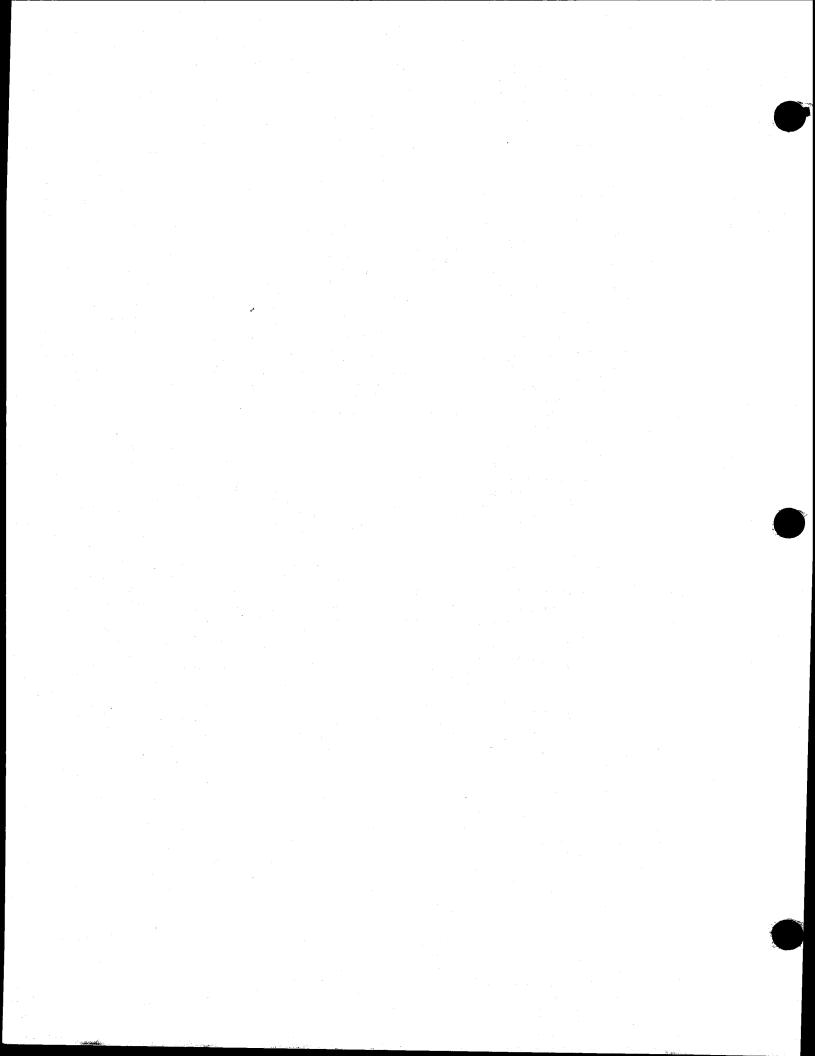
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SECTION I

General Information

- 1-1. Description.
- 1-2. The ATC-1200Y3 is a civil transponder and DME test instrument designed to meet the functional test requirements of a pulse test station. Only a high-quality, dual-trace oscilloscope and a counter are needed in addition to the ATC-1200Y3.
- 1-3. The ATC-1200Y3 is equally at home testing the simplest DME, or the sophisticated ARINC transponder or DME of latest design. Transponder tests feature interrogation in all modes including A/C, rapid setting of transmitter frequency and measurement of transmitter power. Receiver sensitivity checks are accurate and fast using the convenient front panel display of % reply.
- 1-4. DME tests include accurate range measurements in 0.01 mile steps to 999.89 miles and equally accurate velocity measurements in 10 KT steps to 9990 KTS. Both are crystal controlled. Tests to measure transmitter frequency, transmitter power, decoder window limits and receiver sensitivity are all front panel functions.
- 1-5. The built-in L-Band signal generator covers the spectrum of 950 1225 MHz. It may be operated in any of three modes: a) a crystal controlled, phase-locked generator with direct frequency readout, b) a crystal controlled, phase-locked generator with paired VOR channel readout, or c) as a continuously variable frequency generator from 950 1225 MHz. A CW function allows the test set to be used as a general purpose L-Band generator of high stability and including an accurate output attenuator.
- 1-6. Warranty. (See following page)



SECTION II

Specifications

and

Technical Summary

Transponder Section

Interrogation Rate:

Variable from 50 Hz to 5000 Hz. PRF control accuracy ±5%.

Interrogation Modes:

A/C, A, B, C, and D, per FAA TSO C-74a. Pulse spacing relative to leading edge of Pl:

Mode A 8us ±0.05us Mode B 17us ±0.06us Mode C 21us ±0.06us Mode D 25us ±0.08us Mode A/C 8us ±0.06us 21us ±0.08us

Transponder Pulse Characteristics:

Pulse rise times should be 100ns or less for P1, P2 and P3. When the leading edge of P2 is within 0.6us or less of the trailing edge of P1, the rise time of P2 degrades to greater than 100ns. If P2 is within 0.3us of the trailing edge of P1, and P1 and P2 will deform. P2 may vanish.

Variable Pulse Spacing:

P2 and P3 variable ±1.0us from each nominal position. Control accuracy ±0.05us at 0 setting and ±0.1us at +1 and -1us settings.

Variable Pulse Width:

Variable width (of all three pulses simultaneously) from 0.4us to 1.2us. Control accuracy ±0.05us.

Side Lobe Suppression:

Side Lobe pulse spaced 2us relative to Pl. Spacing accuracy ±0.05us. Variable in amplitude relative to Pl from -10dB to +1dB, control accuracy ±.5dB at +1dB and 0dB; and ±1dB at -6 and -10dB. P2 pulse may be turned off.

Pre Pulse:

Selectable On or Off by Front Panel switch. Equal in Amplitude and Width to Pl and P3. Time before Pl adjustable to 5us by the CAL Ø control

Calibration Mark Gen:

Crystal controlled 1.0us or 1.45us time marks. Crystal tolerance ±.01%. lus frequency = 1 MHz. 1.45us frequency = .689650 MHz. Output pulse amplitude adjustable to 1V P-P with 51 ohm load.

Sync Pulses:

T_O: Negative sync pulses are provided approximately 5us prior to the leading edge of Pl.

T_D: Negative sync pulses are provided on the leading edge P3 for monitoring of all reply pulses.

Nominal amplitude is -15V. Pulse width is 0.5 to 3us.

Transmitter Frequency Check:

Transmitter frequency is measured by heterodyne method through diode mixers. Frequency settable to 500 kHz at 1090 MHz.

Transmitter RF Power:

Measured by calibrated slide-back power meter. Power at any point of the reply pulse may be measured. Accuracy of power control is 12% at 2.5 kW and 15% at 50 watts.

Transponder % Reply:

Meter readout 0 to 100% Accuracy ±2%.

Suppressor Pulse:

Coincident with Pl of interrogation pulse train. Pulse width is 50us, ±2us. Amplitude nominal 19 V, ±1 V.

Interrogation RF Pulse Risetime:

Less than 100 ns. Overshoot 5% maximum.

Interrogation RF Pulse Decay Time:

Less than 100ns.

RF On/Off Ratio:

DME SECTION

Squitter:

Ident System:

Sync System:

Range System:

80dB minimum, 85dB typical.

Rate of pulse pairs is variable from average of 50Hz to 5000Hz. Squitter has completely random time distribution. Average rate accuracy: ±3.5%.

Provides constant ident tone or coded IDENT signal. Tone frequency is 1350Hz, ±1%. Ident equalizing pulse is spaced 100us from first pulse. Spacing accuracy: ±3us. IDENT signal is available every 30 seconds, ±2 sec., of characters I-F-R. Speed: approximately 7 WPM.

ro: Negative sync pulses are provided approximately lus after time of input interrogation.

TD: Sync Range - Negative sync pulses are provided (approximately 5us before) with each range reply pulse to permit viewing the reply pulses.

Sync Squitter - Negative sync pulses are provided at leading edge of Pl pulse to permit viewing squitter pulses.

Nominal amplitude of all. sync pulses is -15 V. Pulse width is 2 to 15us.

Provides crystal controlled fixed range distances from -1 mile to 999.89 N.M. in 0.01 N.M. selectable increments. Range accuracy: ±0.025 miles, ±.005% of range.

Velocity System:

Crystal controlled velocity rates from 0 to 9990 KTS, in 10KT selectable increments. Velocity accuracy 0.02%. Velocity range 0 to 300 N.M. with meter readout. Range readout accuracy ±5 N.M. Electrical slewing 0 to 300 N.M. in approximately 6 sec.

NOTE

Due to discrete range steps in Velocity mode of .01 mile and to range jitter of .01 mile max, the maximum range uncertainity is .02 mile when measuring velocity on a time interval counter. If the range-change verses time measurement is made at 1000 knots for 60 seconds, the maximum velocity error due to the .02 mile uncertainty is ±0.12%. See table below.

A. When measuring at a 60 second time interval:

Velocity	Maximum Error
100	1.2%
200	0.6%
500	0.24%
1000	0.12%
5000	0.024%

B. When measuring at a 30 second time interval:

Velocity	Maximum Error
100	2.4%
200	1.2%
500	0.48%
1000	0.48%
5000	0.048%

C. When measuring at a 10 second time interval:

Velocity	Maximum Error
100	7.2%
200	3.6%
500	1.44%
1000	0.72%
5000	0.144%

Percent Reply:

Random Reply elimination with average count down rate variable from 20% to 100% replies. Control accuracy ±5%.

Tacan Simulation:

Simulation only by amplitude modulating all output pulses with 60Hz. Modulation level variable from 0 to 50%.

Suppressor Pulse:

Output rate is a constant value controlled by Squitter PRF control. Pulse width is 50us ±2us. Amplitude nominal 19V ±1V.

R-NAV Pulses:

P1 at time of interrogation; P2 at time of reply. Pulse spacing at 0 miles is 50 us in X ch. ± 0.25 us, and 56us in Y ch, ± 0.25 us. Pulse width is 7us, ± 3 us, amplitude 15 v, ± 3 V.

Decoder:

An input decoder is incorporated which will accept input pulse pairs only with spacings between:

in X ch - 8.5us to 15.5us ± 0.5 us. in Y ch - 33.5us to 38.5us ± 1.0 us

DME Pulse Widths Characteristics:

DME pulse widths should be $3.5us\pm0.25us$ when on a frequency of 1030 MHz. Typical pulse width variation with frequency is $\pm0.5us$. For "X" channel operation the spacing cannot be operated in the -4us, -5us or -6us position without severe pulse distortion because P1 and P2 are being overlapped.

Output Pulse Spacing:

In X channel 12us, ±0.2us. In Y channel 30us, ±0.2us. Pulse spacing is adjustable from nominal 12 or 30us in ±0.5, ±3, ±4, ±5 and ±6us steps. Accuracy of incremental spacing is ±0.2us. X or Y channel spacing by VOR frequency selected.

Echo Pulses:

Echo Pulse pair injected 30 N.M. from time of interrogation.
Range accuracy of echo pulses ±0.5 N.M. Echo pulse amplitude variable from -10 dB to +1dB, control accuracy ±0.5 dB at -10 dB, -6 dB, 0 dB, and +1 dB, relative to normal reply pulse. Normal reply pulses cannot be used within ±5 N.M. of echo pulses. Echo pulse pair may be turned off. All output pulses are square instead of Gaussian shaped when the echo system is activated.

PRF Measurement:

Interrogation rate of DME read out on meter on 0-30 and 0-300 PRF ranges. PRF accuracy ±3% full scale.

Modulator Pulse Output:

Gaussian-shaped reply pulse pair timed within ±0.3us of RF reply pulses. Amplitude adjustable from 0 V to -10.5 V. D.C. restored to peak of 0 V. Spacing same as RF pulses.

Transmitter Frequency Check:

Transmitter frequency is measured by heterodyne method through diode mixers. Used only to verify proper on-channel frequency to ±1 MHz.

Transmitter RF Power:

Measured by calibrated slide-back power meter. Power at any point of the interrogate pulse may be measured. Accuracy of power control is 12% at 2.5 kW and 15% at 50 watts.

DME RF pulse output:

Gaussian-shaped reply pulses 3.5us, ±0.25us, wide at 50% amplitude point.

RF On/Off Ratio:

85 dB minimum, 95 dB typical.

Signal Generator Section

Frequency:

Frequency Control:

Output Leveling:

950 MHz to 1225 MHz

- 1. In GHz position, the front panel frequency switch indicates generator frequency directly in MHz providing decimal point is considered invalid. Phase lock range typically 960 MHz to 1215 MHz. Frequency selected in 1 MHz. increments. Output frequency accuracy ±.008%. DME spacing always X ch in GHz mode.
- 2. Paired VOR channel readout:
 Front panel frequencies switch indicates VOR frequencies from 108.00 to 117.95 MHz, and 133.30 to 135.95 MHz selectable in 50 kHz increments.
 Output frequency from 962 MHz to 1213 MHz paired to VOR channels. Phase lock range 962 to 1213 MHz. Output frequency accuracy ±.008%. All XXX.00 channels select X ch. spacing; all XXX.05 channels select Y ch. spacing.
- 3. Variable Frequency: Range 950 MHz to 1225 MHz, Drift rate typically less than 2.0 MHz in a one-hour period. An external counter capable of counting 3.25 MHz can display the output frequency. Add 9 MHz to the counter reading and multiply the sum by 100 to obtain the output frequency.

For sets S/N 1500 and on, RF output leveled to ±1.0dB for any one attenuator setting in 962 to 1213 MHz frequency range. For sets prior to S/N 1500, RF output leveled to ±2.0 dB for any one attenuator setting over frequency range 962 to 1213 MHz.

RF Output Level:

Continuously variable from 0 dBm to -110 dBm. Attenuator accuracy ±1.5 dB referenced to Output Leveling. Output level is calibrated at XMTR/REC connector. Harmonic content of output 70 dB down from attenuator is non-linear from 0 dBm to -30 dBm. Use of attenuator calibration curve is mandatory for this region of operation.

General

AC Power Requirements:

105 to 120 VAC or 220 to 250 VAC 50 to 400 Hz. Cooling fan 50/60 Hz only.

Weight:

36 pounds

Dimensions:

7.5" high, 16.75" wide, 18.375" deep.

SECTION II

INSPECTION

- 2-1. Each IFR Precision Simulator is care-INCOMING INSPECTION. fully inspected for mechanical and electrical quality before shipment from the factory. On receipt, the instrument should be physically free of mars and scratches, and in perfect mechanical and electrical order. The instrument should be inspected immediately for possible in-transit physical damage. A check for supplied accessories, and a test of the electrical performance of the instrument (as outlined in Section V of this manual) should also be made. Any damage or deficiency should be reported immediately to the carrier and a claim filed, if necessary. LIMITED WARRANTY AND SERVICE INSTRUCTIONS of this manual for delineation of responsibilities and liabilities. the directions in the LIMITED WARRANTY AND SERVICE INSTRUC-TIONS when it becomes necessary to ship the instrument.
- 2-2. GROUNDING REQUIREMENTS. To protect operating personnel, the National Electrical Manufacturer's Association (NEMA) recommends that the instrument panel and cabinet be grounded. All IFR instruments are equipped with a three-conductor power cord which, when plugged into an appropriate receptacle, grounds the instrument. The offset pin on the power cord three-prong connector is the ground wire.
- 2-2-1. To preserve this protection feature when operating the instrument from a two-contact outlet, use a three-prong to two-prong adapter and connect the green pigtail on the adapter to ground.
- 2-3. CLEANING. It is wise to clean the dust, cobwebs, and other debris out of the test set prior to periodic inspection, repair or calibration. Some shops clean their test equipment on a regular basis such as biannual or annual proofof-performance checks. Annual recalibration of the set is advisable.
- 2-3-1. Dust removal is best done with a hand controlled dry air jet of 25 to 50 psi (1.827 kg/cm² to 3.653 kg/cm²). The Rear Panel should be cleaned with a dry cloth only. The Front Panel may be cleaned whenever necessary with a lint-free cloth moistened with rubbing alcohol.
- 2-3-2. CARE MUST BE TAKEN TO AVOID BREAKING WIRES OR SHORTING COMPONENT LEADS TOGETHER DURING CLEANING.

- 2-7. Repackaging for Shipment.
- 2-8. The following is a general guide for repackaging for shipment. If you have any questions, contact the IFR Shipping Department. (See Section I, Paragraph K)

NOTE	

If the instrument is to be shipped to IFR for service or repair, attach a tag to the instrument identifying the owner and indicating the service or repair to be accomplished; include the model number and full serial number of the instrument. In any correspondence identify the instrument by prefix, model and serial number.

Place instrument in original container if available. If original container is not available, contact IFR for shipping instructions.

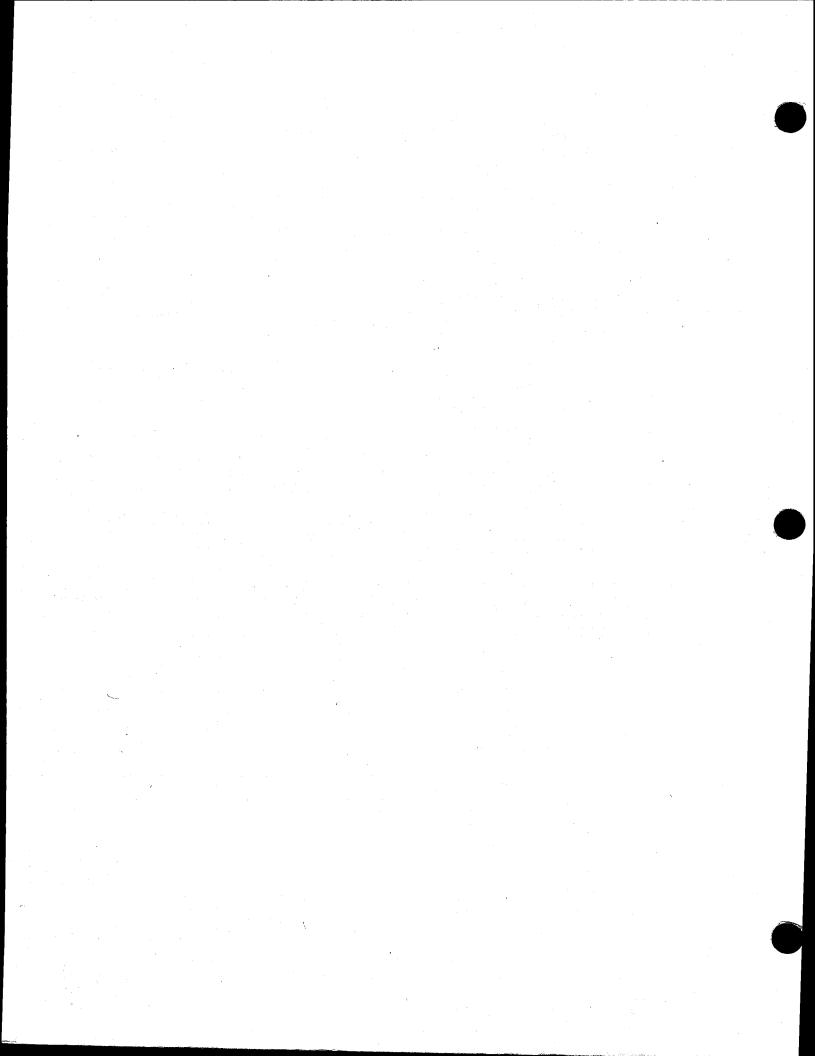
Do not return the instrument or its component parts to IFR, Inc. for repair without first receiving authorization from IFR, Inc. Refer to paragraph 1-H for complete instructions.

- I. <u>Transformer</u>. Inspect the transformer for signs of excessive heating, broken or charred insulation, and loose mounting hardware.
- J. <u>Wiring</u>. Inspect all the wiring of the chassis for broken or loose ends and connections and for proper dress relative to other chassis parts. All the laced wiring should be tight with the ends securely tied.
- 2-5. REPACKING FOR SHIPPING. The LIMITED WARRANTY AND SERVICE INSTRUCTIONS contain detailed directions for repacking and shipping. Additional questions may be directed to the IFR Shipping Department.

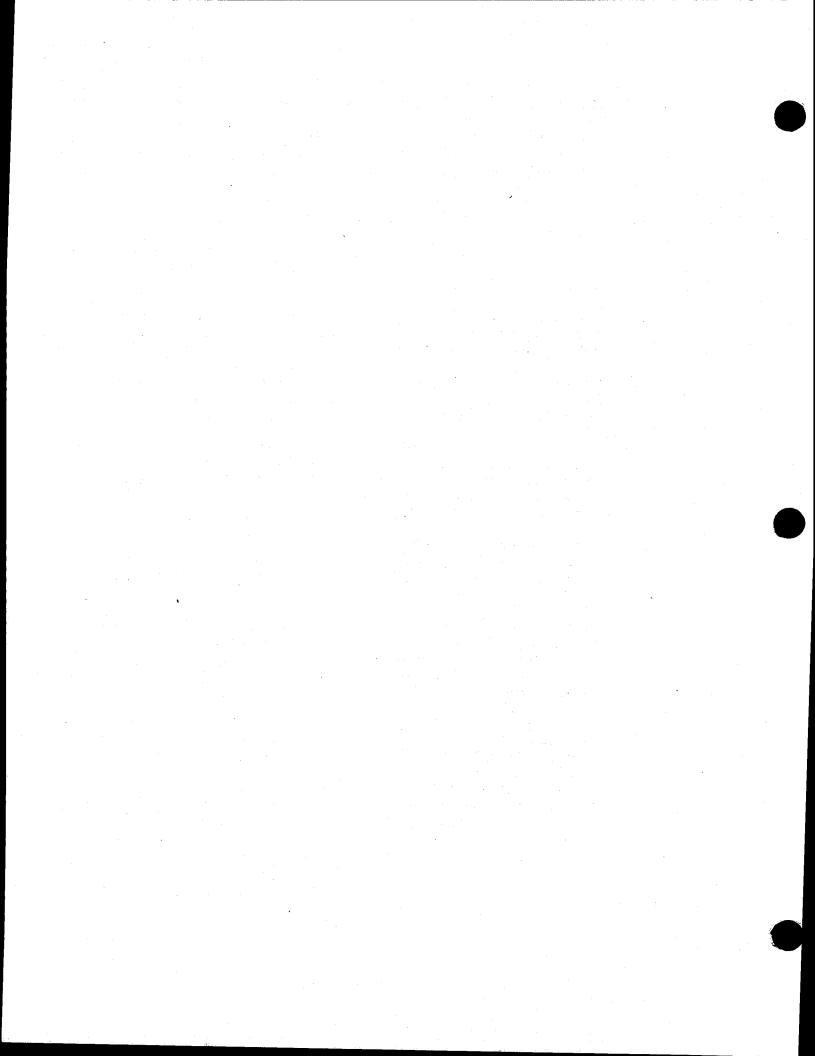
NOTE

Any instrument shipped to IFR for any reason MUST be tagged with (1) its owner's identification, (2) the service or repair required, (3) its model number, and (4) its full serial number. Identify the instrument by prefix, model, and serial number in ALL correspondence.

- 2-5-1. IFR Precision Simulators should be shipped ONLY in their original containers. If the original container is not available, contact IFR for shipping instructions.
- 2-5-2. DO NOT return an instrument or its component parts to IFR without first receiving authorization from the IFR Customer Service Department. Refer to the LIMITED WARRANTY AND SERVICE INSTRUCTIONS for complete directions.



- A. Chassis. Includes anything mechanical or made from metal. Inspect for tightness of sub-assemblies, damaged connectors, corrosion or damage to the metal surfaces, etc. Surface corrosion may indicate damage inside the affected part.
- B. Capacitors. Inspect for loose mounting, body damage, case damage, leakage or corrosion around leads.
- C. Jacks. Inspect all coax jacks for loose or broken parts, cracked insulation, bad contacts, etc. Do not disassemble connectors within the test set.
- D. Potentiometers. Any potentiometer that feels rough when rotated or produces circuit or voltage irregularities should be checked with an ohmmeter for proper operation.
- E. Resistors. Inspect all types of resistors for cracked, broken or charred or blistered bodies and loose or corroded soldering connections.
- F. Printed Circuit Boards. Check connectors for corrosion and damage and the mating plugs for similiar damage. Inspect all mounted componets for damage including crystals and IC's. The board should be free of all foreign material.
- G. Semiconductors. Inspect all diodes, rectifiers and transistors for cracked, broken, charred or discolored bodies. Check ends of components for seals around leads.
- H. Switches. Examine all toggle switches for loose levers and terminals, loose body to frame condition. The line switch contacts should not be bent nor the switch action too loose. The thumbwheel switches should have definate detents and not feel loose.
- I. Transformer. Inspect the transformer for signs of excessive heating, broken or charred insulation, loose mounting hardware and other abnormal conditions.
- J. Wiring. Inspect all wiring of chassis for broken or loose ends and connections and proper dress relative to other chassis parts. All laced wiring should be tight with ends securely tied.



1200Y3 CONTROLS & CONNECTORS & INDICATORS

Front Panel

	Interr./Squitter Rate Control P2 Dev us Control	3 - 6 3 - 7
3.	P3 Dev us Control	3 - 8
4.	Xpdr Pulse Width us Control	3 -9
5.	Mode Switch	3-10
6.	SLS/Echo Level - dB Control	3-11
7.		3-12
8.	DME Pulse P2 Dev us Control	3-13
9.	X1/X10 Prf Switch	3-14
10.	Velocity - KTS Switch	315
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14.	Slew In/Out Switch	3-19
15.	Dist. In/Out Switch Squitter On/Off Switch Ident Off/1350 cycle/Ident on	3 20
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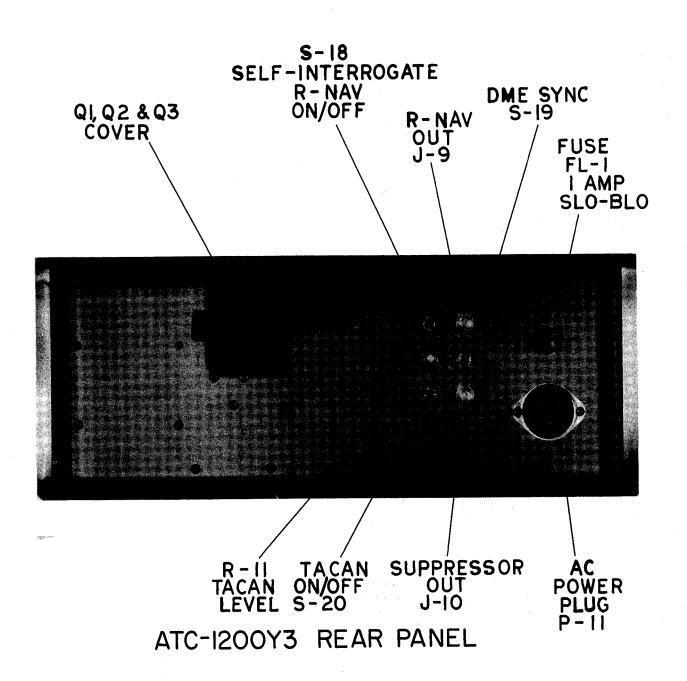
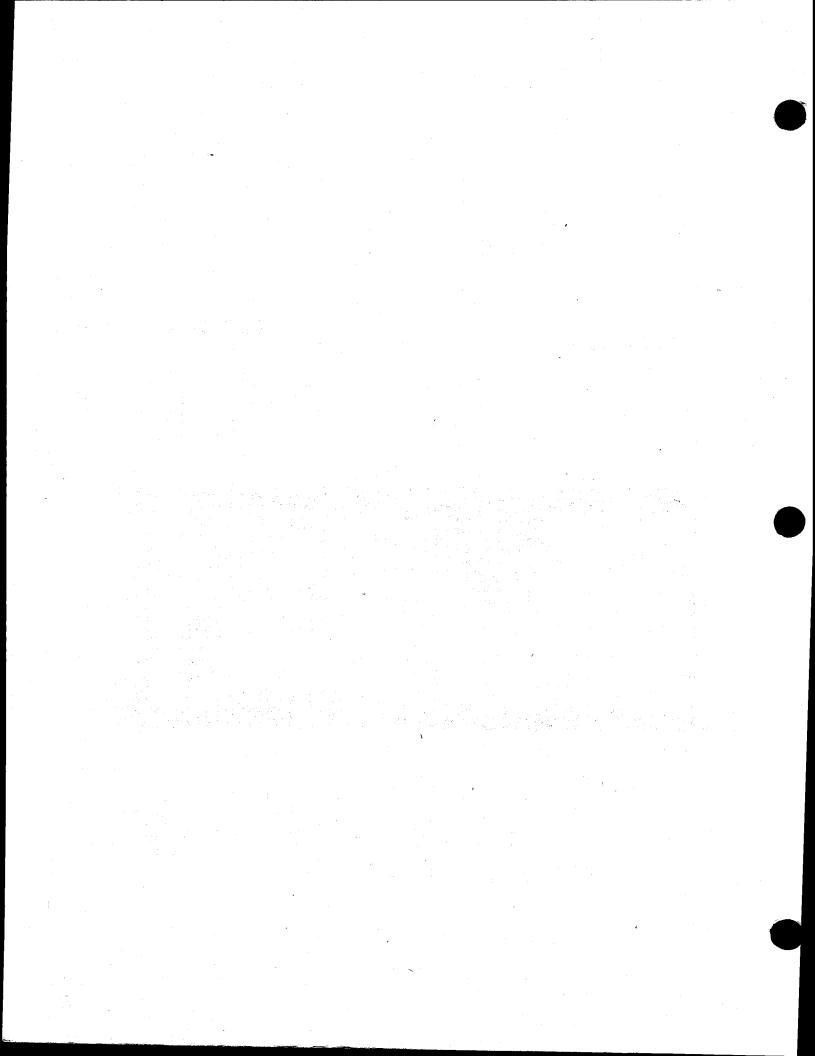


Fig 3-2



SECTION III

Operation

3-1. INTRODUCTION

3-2. The ATC-1200Y3 is a self-contained, complete pulse test instrument for transponder and DME systems. All necessary test signals and their variations are generated with the one set. Only an oscilloscope and counter are required as peripheral equipment.

3-3. CONTROLS, CONNECTORS, AND INDICATORS

3-4. Location of all controls, connectors, and indicators is shown in Figure 3-1 and Figure 3-2. The following paragraphs explain their functions in detail.

3-5. FRONT PANEL

- 3-6. Interr./Squitter Rate Control. Known also as the PRF Control, it varies the frequency of a temperature-stabilized oscillator from 50 to 500 Hz, and 500 to 5000 Hz. The range is selected by the X1/X10 switch directly below the control. See paragraph 3-14. The oscillator is used for three purposes: a) To determine the interrogation rate of a transponder in Transponder Modes of operation, b) to determine the average squitter rate in DME Modes of operation, and c) to determine the interrogation rate of the ATC-1200Y3 itself in R-NAV operation, to permit using the test set as a DME in testing of R-NAV computers. Also when in DME Mode, the control directly determines the rate of suppressor output pulses. See paragraph 3-51, Suppressor Output Connector.
- 3-7. P2 DEV. us Control. The spacing of P2 (SLS pulse) relative to P1 is controlled by the smaller, outer knob of concentric controls. Actual P2 deviation is read relative to the large, inner knob with that knob set to 0.0us deviation. At 0.0 indicated, spacing is 2us, and is variable ±1.2us.
- P3 DEV us Control. The spacing in us of P3 relative to P1 is controlled by the large, inner knob of concentric controls. When at 0.0 indicated, P3 spacing is the nominal time in us commanded by the mode of interrogation A, B, etc. P3 spacing may be varied by ±1.2us from any mode spacing.

- 3-9. XPDR Pulse Width us Control. This control determines the pulse width of Pl, P2, and P3 simultaneously.

 Nominal width is 0.8us, and may be varied from 0.4 to 1.2us.
- 3-10. Mode Switch. The Mode switch controls whether the ATC1200Y3 operation is for Transponder or DME testing.
 Transponder modes are A/C, A, B, C, D, and FREQ. CHECK.
 Interrogation mode is A in frequency check. DME modes
 are DME and DME FREQ. CHECK. In frequency check position
 the internal signal generator is allowed to heterodyne
 with the incoming DME transmitter signal to determine
 the transmitter frequency.
- 3-11. SLS/ECHO Level dB Control. In Transponder modes this control varies the R.F. level of the SLS Pulse, P2, relative to P1 and P3. Control range is +1 to -10 dB. At 0 the P2 level is the same as P1, which is determined by the Output dBm control. See paragraph 3-18. In the OFF position P2 is completely turned off. In DME mode the control turns on or off a pulse pair with the same spacing as the normal reply pulse pair (12 or 30 us) and at a fixed range of 30 miles relative to time of interrogation. In addition the control varies the R.F. level of the echo pulse pair relative to the normal pulse pair from +1 to -10 dB. At 0 the echo pulses are the same amplitude as the normal reply pulses, which is determined by the Output dBm control.
- 3-12. Power KW Control. This control varies the power meter slide-back voltage and is used in measuring both transponder and DME transmitter power levels, either peak or at any other point on the output waveform. The output power is read directly from the control scale when the point on the waveform to be measured is reduced to the base line of an oscilloscope display.
- 3-13. DME Pulse P2 DEV us Control. The DME reply pulse pairs nominally have a spacing of 12 or 30 us. The P2 DEV us control enables the test set operator to vary this spacing to less than nominal (-DEV) or greater than nominal (+DEV). Discrete steps are provided of ±0.5, ±3, ±4, ±5, and ±6us. Pl is the ranging pulse and always remains in nominal position, with P2 changing its position relative to P1.

- 3-14. X1/X10 PRF Switch. The PRF X1/X10 switch changes the dial reading of the Interr./Squitter Rate control by 10 and the frequency of the PRF oscillator by 10. See paragraph 3-6.
- 3-15. VELOCITY-KTS Switch. This switch determines the velocity rate the test set is simulating when in velocity mode. Velocity rates are in 10KT increments from 0 to 9990 KTS. Velocity range and inbound or outbound directions are determined by other controls. See paragraph 3-19 and 3-20. Velocity mode is selected by the Range/Velocity switch, paragraph 3-32.
- 3-16.Frequency Switch. The Frequency switch controls the signal generator frequency in phase-locked operation, and also determines generator frequency readout mode and DME X or Y channel reply spacing. The four left digits always select frequency. The right digit selects the mode. When in 0 position, the switch readout will be VOR paired frequencies from 108.00 thru 117.90 and 133.00 to 135.90 MHz, and the test set will be in X ch. DME reply spacing (12 us). When in 5 position, the readout is also in VOR paired frequencies only from 108.05 to 117.95 and 133.05 to 135.95 MHz (50 KHz spacing channels), and the test set will be in Y ch. DME reply spacing (30 us). When in Gz position, the readout decimal point must be moved mentally two places to the left, and the resultant display will be the output frequency in Gz. In this mode, the generator covers from .960 to 1.215 Gz. The Gz position is normally used for transponder modes but if used in DME mode (for frequency check for other purposes), the DME reply spacing is always X ch. (12 us).
- 3-17. Distance Switch. The precise range delay from interrogation to reply is selected by the Distance switches, Range distances are selected in 0.01 mile steps from 0 to 999.89 N.M. The switch is used only in fixed Range mode selected by the Range/Velocity switch, paragraph 3-32.
- 3-18. Output/dBm Control. This is the output R.F. level attenuator for the internal signal generator. The level is calibrated in -dBm normally used in transponder and DME work, and the calibration is accurate only from -30 dBm to -110 dBm. An attenuator correction curve is provided for each serial number test set for the non-linear region from -30 dBm to 0 dBm, or the low attenuation stop.

- 3-19. Slew In/Out Switch. The Slew switch rapidly moves the DME reply pulses to any range from 0 to 300 N.M., slewing inbound or outbound, when operating in velocity mode. As soon as the switch is released, the velocity switch takes over moving the reply pulses at the programmed velocity setting. Slewing from 0 to 300 miles takes approximately 6 seconds.
- 3-20. Dist. In/Out Switch. When in velocity operating mode, the Dist. In/Out switch controls whether the reply pulses will move toward 0 N.M.-inbound, or toward 300 N.M.-outbound. The rate will be determined by the velocity switch. It should be noted that when operating near either limit, when the range actually reaches the limit it will at once jump to the opposite limit and continue its original course in or out.
- 3-21. Squitter On/Off Switch. This switch turns the squitter pulses on or off. The average squitter rate is determined by the Interr./Squitter Rate control. See paragraph 3-6.
- 3-22. Ident Off/1350 cycle/Ident On Switch. The three position Ident switch a) turns off all ident signals or tones far left position, b) turns on a steady 1350 cycle tone center position, and c) turns on an Ident signal in code at approximately 7WPM of the characters IFR far right position. The signal is repeated every 30 sec. Since when ident is on either continuously or in code it overrides and eliminates all reply and squitter pulses, a warning indicator is lighted continuously in center switch position and in coded form every 30 seconds in right switch position. See paragraph 3-44.
- 3-23. PRF Switch 0-30/0-300. The PRF range switch controls the meter full-scale sensitivity when reading DME interrogation PRF rates. The 0-300 N.M. meter scale and its calibrations are used. The 0-30 PRF range is normally used for DME track PRF's; the 0-300 PRF range is used for DME search PRF's. Input to the PRF measurement system is internal and requires no external, additional connections.
- 3-24. Sync Selector Switch. The Sync switch selects the source of sync signal to be presented to the neg. sync. output connector (paragraph 3-35) to permit viewing various signals concerning test operations. See the Technical Specifications for TO and TD positions in both transponder (page 2-2) and DME (page 2-3) modes. Note also that in DME mode, TD position, a rear panel switch determines actual output sync. See paragraph 3-48.

- 3-25. Cal 1.0/1.45us Switch. This selects the calibrate pulse output signal between 1.0us and 1.45us intervals. Both pulse trains are used only in transponder mode, or during DME calibration procedures of the ATC-1200Y3 itself. The 1.0us is used to monitor spacing of Xpdr interrogation pulses and the 1.45us is used to monitor spacing of reply pulses. See also paragraph 3-26 and 3-36.
- 3-26. Cal Phase (Ø) Control. This control varies the phase between the interrogate and CAL pulses, or the reply and CAL pulses. Total phase variance is approximately 3.5us. The control is used to accurately align the CAL pulses with the leading edge of the interrogation or reply pulses. (See also paragraph 3-46).
- 3-27. DME % Reply Control. The % Reply Control controls the percent of return of reply pulses of the ATC-1200Y3 to an interrogating DME. The % reply can be varied from 20 to 100 percent. The reply pulse drop-out is at a completely random rate determined by an internal noise generator, and so simulates actual ground-to-air propagation path conditions.
- 3-28. VAR or FREQ Switch. The VAR or FREQ switch determines the signal generator mode of operation between a) phase-locked-frequency controlled by the Frequency Switch in FREQ position, see paragraph 3-16, or b) continuously variable frequency operation controlled by the variable frequency sweep controls in VAR position, see paragraph 3-29. In VAR position the generator frequency must be monitored by an external counter.
- 3-29. Variable Frequency Sweep Controls. Two controls are used to vary the signal generator frequency when in VAR mode. (Paragraph 3-28) A coarse control the large, outer knob will sweep the output frequency from 950 to 1225 MHz. The fine adjust control the small, outer knob will sweep the frequency approximately 1.5 to 2.5 MHz over its full range.
- 3-30. -1 Mile Switch. When turned on the -1 mile switch will subtract an exact one mile from whatever range the test set is replying at, whether in range or velocity mode. If the range switches are at 0 miles the output range will be -1 mile, enabling the operator to test steps on drum DME readouts, etc.

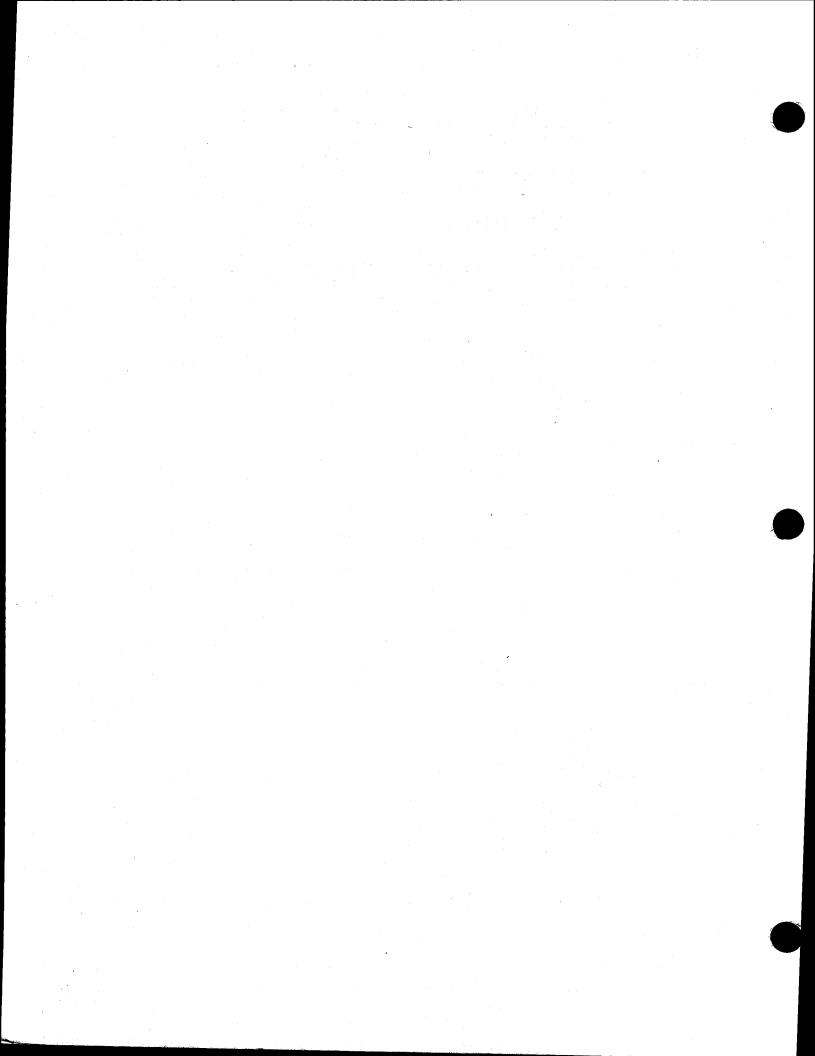
- 3-31. CW Switch. The CW switch disables both the ON-Off and Shaping modulators and applies CW R.F. energy to the XMTR/REC jack at the level set by the Output -dBm control. Frequency of output may be determined any one of three ways: a) phase-locked direct frequency readout, b) phase-locked VOR paired channel readout, or c) variable frequency control over the band from 950 to 1225 MHz. See paragraph 3-16 and paragraph 3-28 and 3-29.
- Range/Velocity Switch. This switch selects between the two modes of DME Test operation of the ATC-1200Y3. Range mode gives a stationary, accurate range selected by the Distance switch. Velocity mode gives a range changing at a precision rate selected by the Velocity -KTS switch. See also paragraph 3-15 and paragraph 3-17.
- 3-33. Line Switch. Applies AC power to test set.
- 3-34. Test Input Connector. The Test Input is the input to the decoder, and is designed to be used as a twin-pulse generator test and alignment input. If the test generator is synced with the ATC-1200Y3 via an internal test point, the lus CAL pulse train will be stationary with respect to the interrogate and reply pulses and enable test set alignment to be easily accomplished.
- 3-35. Negative Sync Output Connector. The Negative Sync Pulse generated by the test set is presented at this connector to keep an oscilloscope in time with the various input and output signals. See also paragraph 3-24 and the Technical Summary under transponder and DME sync outputs.
- 3-36. CAL us Output Connector. The 1.0us or 1.45us pulse trains are presented at this connector for timing measurement of various signals. The connecting coax should be terminated in 50 ohm at the oscilloscope end.
- 3-37. Modulation Output Connector. DME shaped pulses closely coincident with the R.F. reply pulses are presented for use in modulating an I.F. generator or applying directly to a DME's ranging circuits. They are positive in amplitude (0 to 10.5 V P-P) and D.C. restored at the top of the pulses to zero volts. See Technical Summary.
- 3-38. Counter Output Connector. The output pulses direct from the counter block are presented here for determining the signal generator frequency in variable frequency mode

and to be observed on an oscilloscope periodically for pulse stability in the counter chain. To determine the output R.F. frequency, add 9 MHz to the counter reading and multiply the sum by 100.

- 3-39. Generator Monitor Connector. The R.F. pulses generated by the ATC-1200Y3 are detected, amplified and presented at this monitor connector to enable viewing the interrogation to a transponder or reply and squitter to a DME. Generally the output R.F. level should be relatively great to view these pulses. The connecting coax should be terminated in 50 ohm at the oscilloscope end.
- 3-40. Power Monitor Connector. This connector will present all pulses coming into the ATC-1200Y3. All power and frequency measurements are performed by observing these pulses. The connecting coax should be terminated in 50 ohm at the oscilloscope end.
- 3-41. XMTR/REC Connector. All RF pulses coming into or going out of the test set pass through this connector. The output -dBm control is calibrated at this connector into a 50 ohm load.
- 3-42. Signal Generator Phase Lock Indicator. Whenever the signal generator is placed in phase-lock mode and the frequency switch is set between the limits the generator will phase lock in, this indicator must be lighted. It indicates the generator is in control of the phase lock circuitry. When in variable mode, if the generator frequency is manually set at the same frequency the frequency switch is set at, the indicator may flash on and off. This is normal operation.
- 3-43. Echo On Indicator. The Echo On Indicator warns the operator he has an echo pulse pair present in the output to a DME under test which could enable him to wrongly adjust the ranging circuits. See paragraph 3-11. When echo is on, all output pulses are square instead of Gaussian shaped. This will cause the normal range to decrease by approximately 0.1 mile.
- 3-44. Ident/Self Interrogate Indicator. This indicator warns the operator that either the Ident tone has been left "on" (which will override all range pulses) or the R-NAV On/Off switch is on thus generating many false replies. The indicator will flash the code characters I-F-R when the ident switch is in the "Ident On" position.

- 3-45. Meter. The 0 to 300 N.M. scale is used for range readout when in velocity mode. It is also used as 0 to 30 or 0 to 300 PRF ranges when in range mode. The blue area of the left one third scale is used to read transponder percent return from 0 to 100 percent. Percent return is automatically computed within the test set with a transponder operating into it. See also paragraph 3-18.
- 3-46. Pre-Pulse On-Off Switch. This toggle switch is used to enable the circuitry which generates the Pre-Pulse. This pulse is similar in amplitude and width to the normal interrogation pulses, Pl and P3. Its relationship in time preceding Pl may be altered by the CAL Ø us control. (See 3-26)
- 3-47. R-NAV On/Off Switch. This switch interrogates the ATC-1200Y3 at the rate set by the Interr/Squitter Rate Control (self-interrogate function). This feature enables the test set to operate an R-NAV computer without having a DME operating into it.
- 3-48. Sync Squitter/Sync Range Switch. When in DME mode, TD sync, this switch selects the output sync between squitter pulses or range reply pulses. The switch is inoperative in TO sync.
- 3-49. Tacan On/Off Switch. Turns on or off a 60 Hz signal used to amplitude modulate all output DME pulses to simulate TACAN modulation. See paragraph 3-52.
- 3-50. R-NAV Output Connector. R-NAV computers requiring two pulses for range information may be operated by the ATC-1200Y3 through this connector. One pulse is at time of interrogation, the other at time of reply. See also paragraph 3-47.
- 3-51. Suppressor Output Connector. Suppressor output pulses for both transponder and DME are presented here. Transponder pulses are coincident with each interrogation pulse, and DME pulses are at a steady rate set into the Interr/Squitter Rate control.
- 3-52. Tacan Level Control. When Tacan modulation is turned on (simulation only), the Level Control varies the percent of modulation from 0 to more than 50 percent. This must be adjusted by observing the video pulses in a DME with a linear video output.

- 3-53. <u>Fuse</u>. This fuse is in the transformer primary winding. Its normal value is 1 Amp.
- 3-54. AC Power Connector. Applies AC power to the test set. Requires a grounding-type cable and plug.
- 3-55. Internal Controls.
- 3-56. There are no internal controls useful during operation. Only calibration and alignment adjustments are internal and require very careful attention when being set. See the maintenance section of this manual for details.



SECTION IV

ATC-1200Y3 Operation Procedures

4-1. INTRODUCTION

- 4-2. The ATC-1200Y3 was designed throughout for maximum operator's convenience and speed, while simultaneously giving him maximum accuracy of test measurements. The only equipment required external of the test set is a high-quality oscilloscope and a counter capable of 3.5 MHz. Connections to these pieces of test equipment are simple and require minimum changing during different testing operations. All R.F. signals and proper modulation signals are developed within the ATC-1200Y3 and are instantly selectable and/or variable to meet the test conditions at hand for transponder and DME work.
- 4-3. The following procedures provide information necessary to operate the ATC-1200Y3 in Transponder and DME modes. The set-ups are given to familiarize the operator with the test set versatility and typical measurement procedures. Refer to Section Three for detailed control functions.

4-4. TRANSPONDER OPERATION

- 4-5. Equipment Set-up. The ATC-1200Y3 is connected to the oscilloscope and the transponder under test as shown in Figure 4-1. All connecting cables are RG-58 50 ohm coax except the R.F. cable which is recommended to be RG-8 foam coax of shortest practical length.
- 4-6. To obtain accurate pulse wave shape determination the cables used for the monitor and CAL pulse outputs should be terminated in 50 ohms at the oscilloscope end. Commonly used is a BNC Tee connector with a 51 ohm resistor in the open end of the Tee, or solder a 51 ohm resistor inside a UG-88 BNC male connector to plug on the Tee.
- 4-7. Some operators have found they can, in some operations, leave the CAL pulse cable unterminated. This produces sharp overshoots on the pulse leading edges and gives a very definite point to time from. It does in no way degrade the accuracy of the signal.

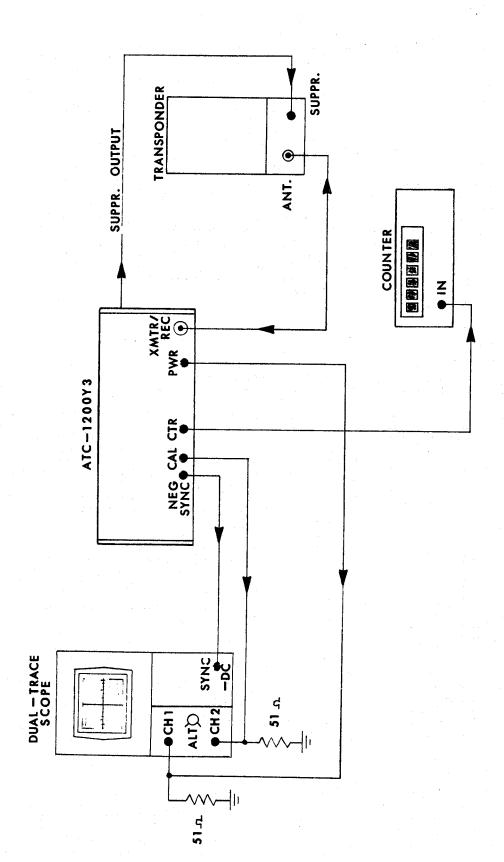


Figure 4-1
Equipment Interconnections
for Transponder Testing

4-8. ATC-1200Y3 Initial Control Settings

- a. MODE SWITCH to A
- b. FREQUENCY SWITCH to 1030 Gz
- c. OUTPUT dBm control to -50 dBm
- d. INTERR/SQUITTER RATE control to 50
- e. X1/X10 SWITCH to X10
- f. Both P2 and P3 DEV us controls to 0.0
- g. XPDR PULSE WIDTH us control to 0.8us
- h. SLS/ECHO LEVEL -dB control to OFF
- i. POWER KW control full CCW
- j. TO/TD switch to TD
- k. CAL us switch to 1.45us
- 1. VAR or FREQ switch to FREQ
- m. CW switch OFF
- n. LINE switch ON (red pilot lamps on)
- o. Connect cables as shown in Figure 4-1
- 4-9. Refer to Figure 4-2 and the following control settings for various transponder tests. Each of the tests outlined in paragraph 4-12 is a typical test only and is therefore generalized. Always refer to the calibration and alignment manual for the Transponder being tested for the specific values, settings and tests to be performed.

4-10. Oscilloscope Control Settings

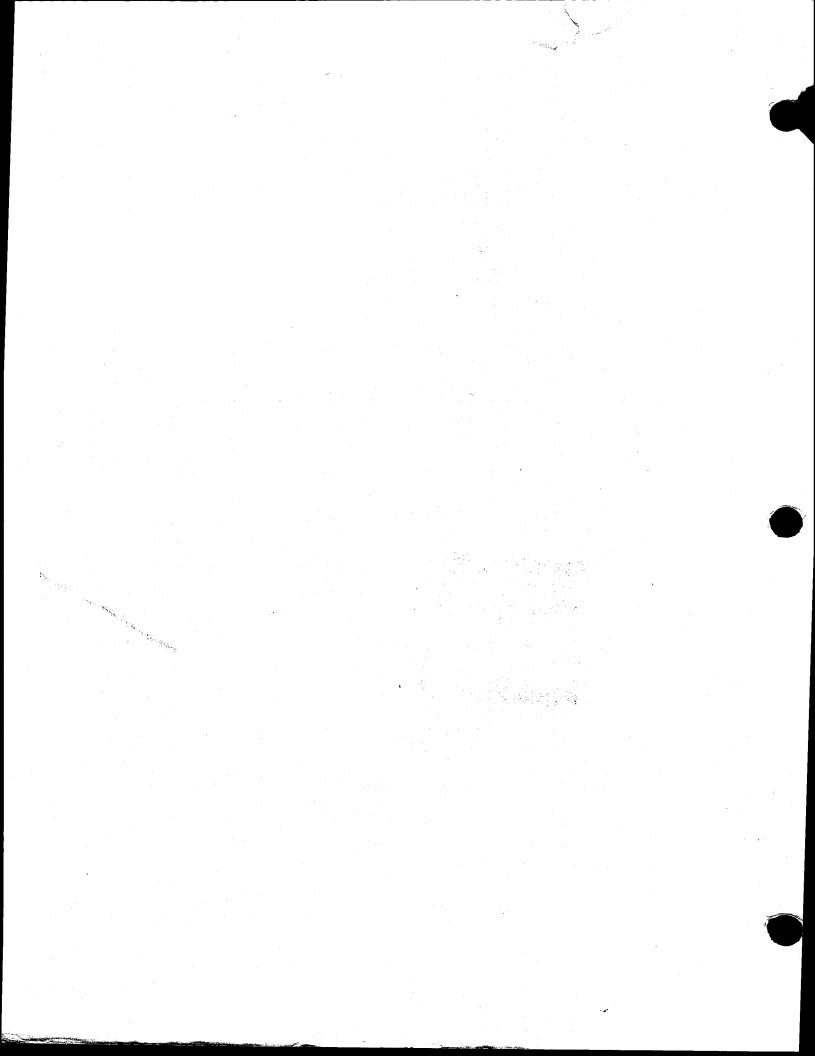
- a. Both vertical gain controls to .05 V/cm
- b. Horiz. sweep to 2 us/cm
- c. Trigger input to EXT, NEG, DC
- d. Intensity as desired for 500 PRF interrogation rate
- e. VERT MODE to alternate.

4-11. Transponder Control Settings

- a. MODE SWITCH to A or A/C
- b. FUNCTION switch to ON (may be same as mode switch)
- c. CODE to 0000

4-12. TYPICAL TRANSPONDER TESTS

4-13. With the controls of the ATC-1200Y3, oscilloscope, and transponder set according to paragraphs 4-8, 4-9, and 4-10, an oscilloscope display should be observed of the transponder reply pulses. Varying the POWER KW control will change the amplitude of the reply pulses, and vary-



ing the CAL \emptyset control will change the relative phasing of the CAL pulses to the reply pulses. These two simple tests indicate proper interconnection of equipment.

A. Sensitivity - Minimum Trigger Level. Interrogate the Transponder at a rate that achieves a solid 100% return with the Output -dBm set to -50 dBm. (This may be other than the 500 PRF as set by paragraph 4-8d and 4-8e). Then reduce the R.F. Output level to achieve 90% return (or per manufacturer's manual) and read MTL reading on the Output -dBm control.

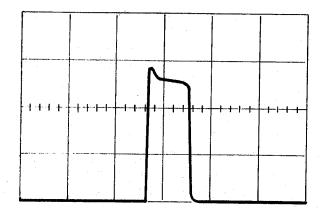
NOTE: The Transponder Percent Return is automatically displayed whenever a transponder is actively operating into the ATC-1200Y3.

- B. Decoder Limits. Vary the P3 DEV us control to determine receiver decoding limits as per manufacturer specs.
- C. SLS Calibration. Turn SLS/ECHO LEVEL -dB control clockwise to ON and set to -10dB. Increase amplitude of SLS pulse (P2) until transponder stops replying to interrogations. This is normally about -6dB return to manufacturer specs.
- D. <u>SLS (P2) Decoder Limits</u>. With the SLS LEVEL control set to no reply from transponder, vary the P2 DEV us control until reply resumes. These + and deviations are the SLS pulse gate limits.
- E. Transmitter Power. Turn SLS LEVEL control to OFF. Turn POWER KW control clockwise until reply pulses just do disappear into the base line of the scope display. Read power in KW directly from POWER KW control scale.

NOTE: Any point on the reply pulse waveform may be measured for power by placing that point on the display base line. Always read power from POWER KW control scale.

F. Transmitter Frequency Check. See Figure 4-3.
Rotate the POWER KW control until approximately 3 cm of reply pulse amplitude is displayed. Next set the ATC-1200Y3 mode switch to FREQ. CHECK. Interrogation

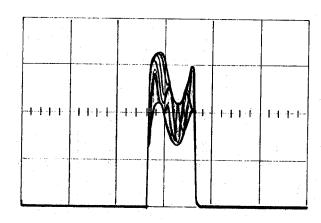
Adjust amplitude with Power - KW Control



Normal Waveform.

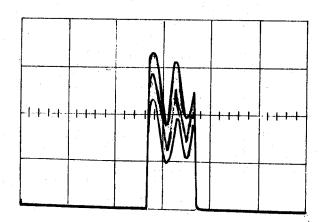
On-Frequency Presentation

Vert: .05 V/cm Horiz: .5 us/cm



Off frequency approximately 1 Mhz (high or low).

Vert: .05 V/cm Horiz: .5 us/cm



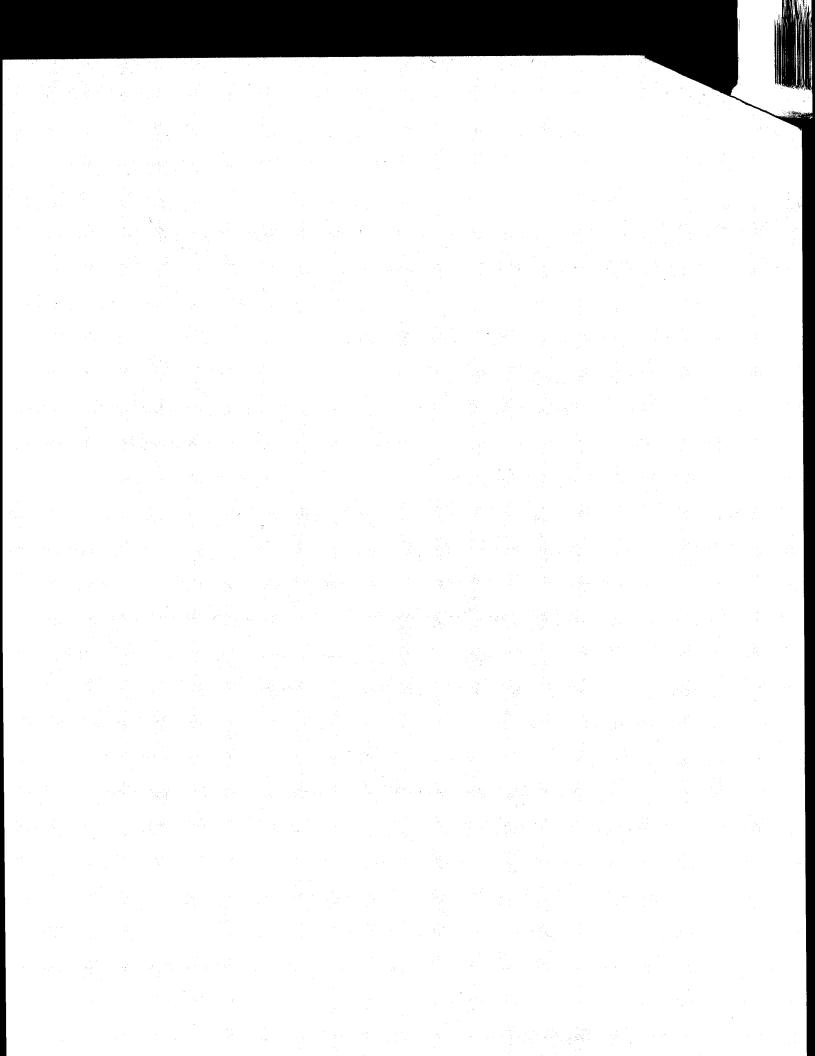
Off frequency approximately 2 Mhz (high or low).

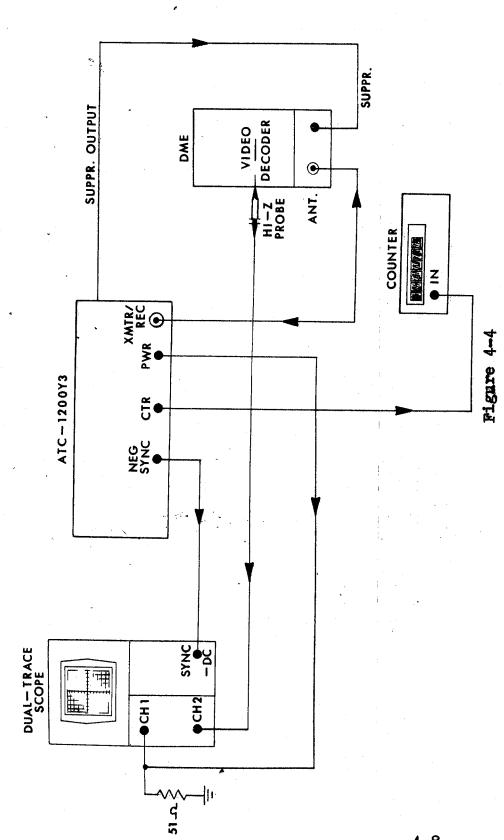
Vert: .05 V.cm Horiz: .5 us/cm

Figure 4-3
Transponder Frequency Check Waveforms

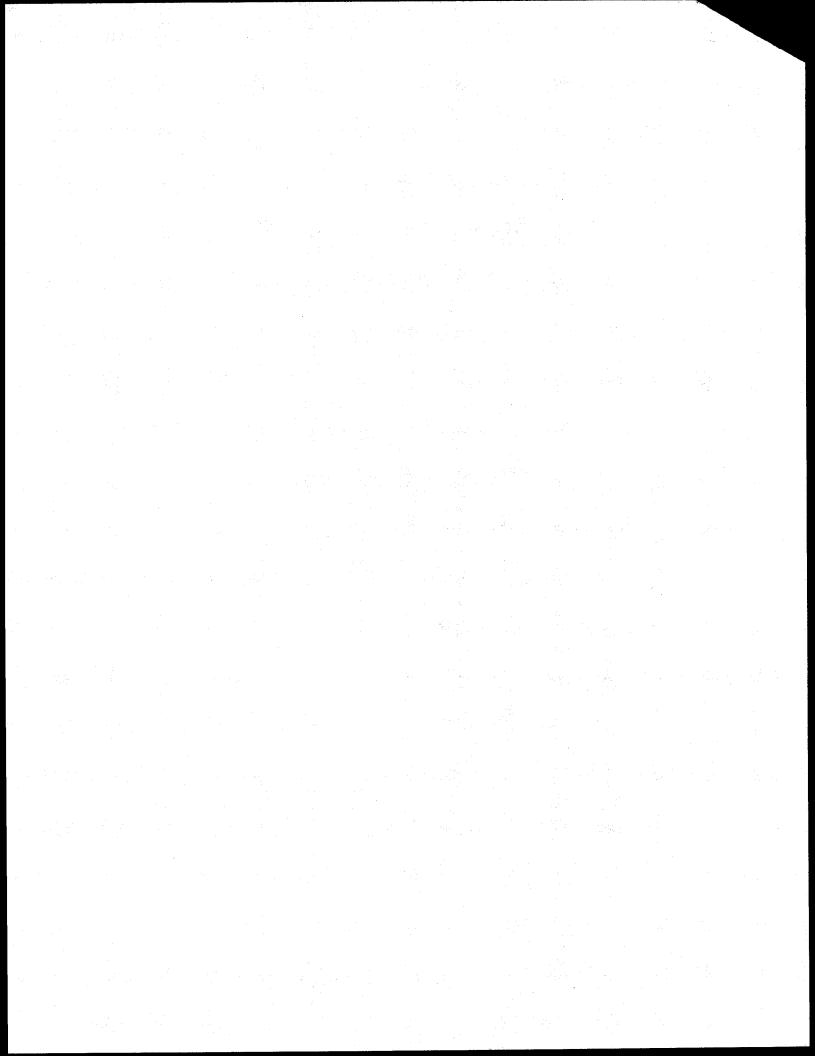
mode will automatically be on mode A. Select 1090 Gz on the FREQUENCY switch. Observe a beat pattern on the reply pulse display. This beat pattern is the result of heterodyning the ATC-1200Y3 signal generator and the transponder transmitter frequencies. Place the VAR or FREQ switch to VAR. Connect a counter to the CTR jack. Using the counter to determine the signal generator frequency sweep the frequency to 1090 MHz. A beat pattern very similar to that obtained in phase-locked operation should be displayed. Use the phase-locked mode to determine transmitter frequency to 1.0 MHz and the VAR mode to determine frequency to 500 kHz or closer, depending on operator experience and skill.

- Reply Pulse Spacing. Set CAL us switch to 1.45 then using the CAL Ø control align the leading edge of any calibrate pulse with the leading edge of Pl of reply. P2 of reply must then occur on the fifteenth CAL mark. Any code set into the transponder must have all pulses of that code occur exactly on the cal mark for that pulse's position. Ident pulse would occur on the eighteenth cal mark after Pl. In addition to checking pulse spacing, the width of the 1.45us pulses is trimmed at the factory for approximately 0.45us the width of the reply pulses.
- H. A/C Mode Interlace. Set Mode switch to A/C. Observe reply pulse on oscilloscope. (Do not use alternate or chopped position). You should see reply pulses at positions A and C with a duty cycle of 50% each.
- I. Suppressor. Operate the ATC-1200Y3 and a transponder as outlined in paragraphs 4-8 through 4-12, observing the reply pulses on the oscilloscope. Next connect a cable between the test set suppressor output and the transponder. All reply pulses should cease while the suppressor pulse is applied to the transponder.
- J. Other Tests. Each manufacturer of ATC Transponder Equipment will have other tests for his specifice requirements. Always utilize the manufacturer's manual and specifications when testing equipment, using the ATC-1200Y3 to provide the test parameters accurately and quickly.

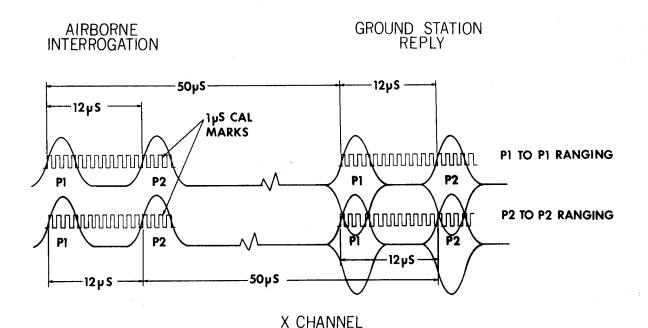


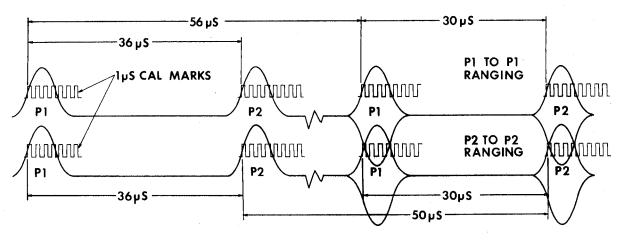


Equipment Interconnections for IME Testing



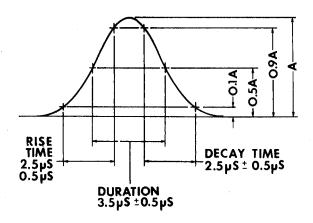
DME PULSE CHARACTERISTICS AND MODE SPACING

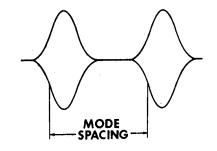




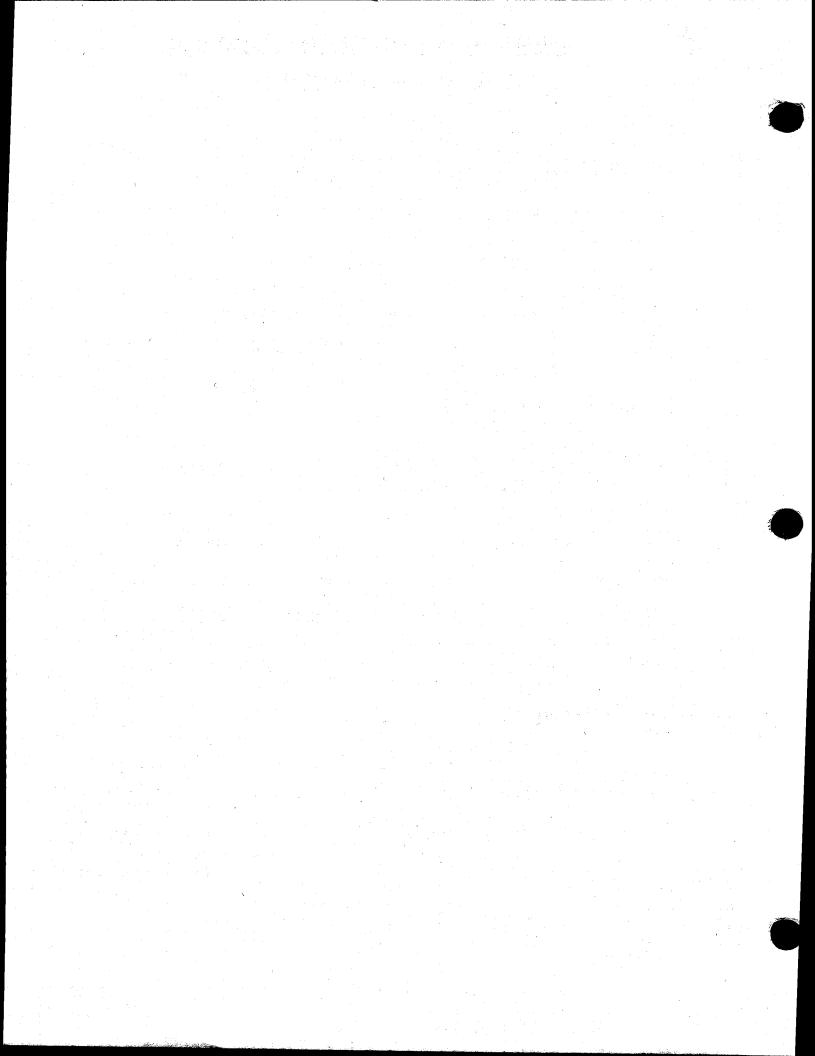
ALL TIMING MEASUREMENTS ARE GIVEN AT 0.5A.

Y CHANNEL





	AIRBORNE INTERR.	GROUND STATION REPLY
MODE	12μS	12µ\$
X	±0.5μS	±0.5µ\$
MODE	36µ\$	30µ\$
Y	±0.5µ\$	±0.5µ\$

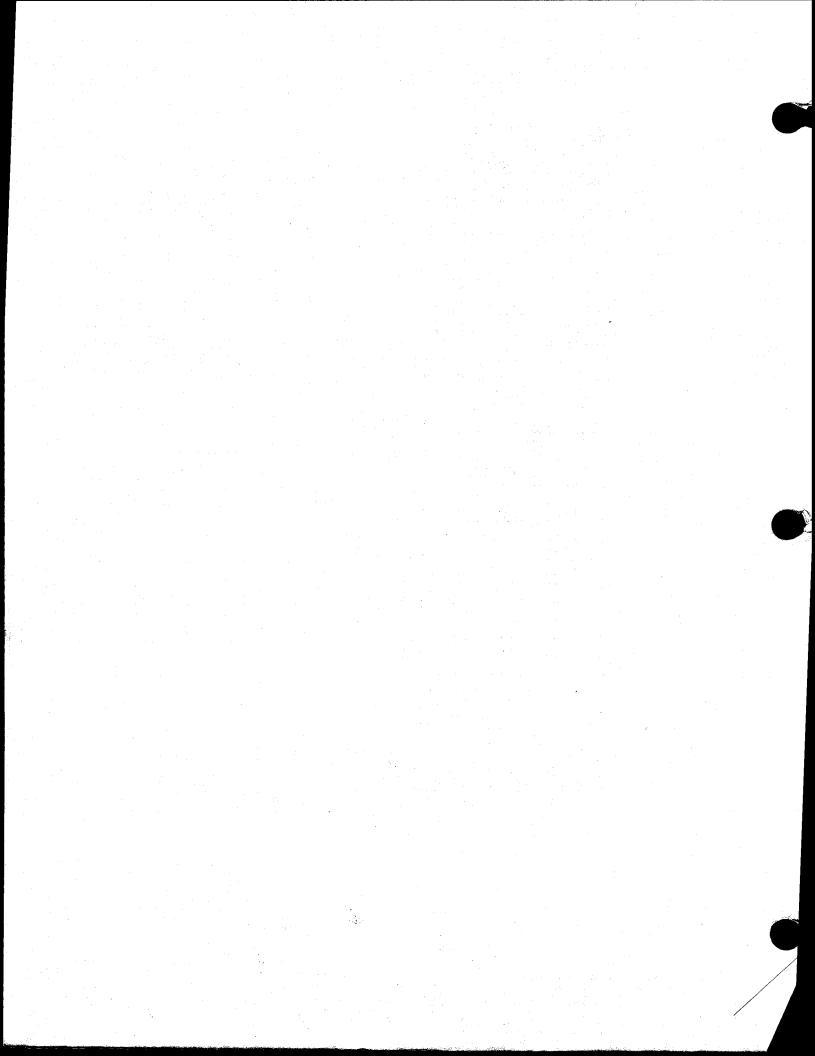


4-14. DME OPERATION

- 4-15. Equipment Set-Up. The ATC-1200Y3 is connected to the oscilloscope and the DME under test as shown in Figure 4-4. All connecting cables are RG-58 50 ohm coax except the R.F. cable which is recommended to be RG-8 foam coax of shortest practical length.
- 4-16. To obtain accurate pulse wave shape determination the cable used for the monitor output should be terminated in 50 ohms.
- 4-17. Refer to Figure 4-5 and the following control settings for various DME tests. Each of the tests outlined in paragraph 4-21 is a typical test only and is therefore generalized. Always refer to the calibration and alignment manual for the DME being tested for the specific values, settings and tests to be performed.

4-18. ATC-1200Y3 Initial Control Settings

- a. MODE switch to DME
- b. FREQUENCY SWITCH to 108.00
- c. OUTPUT -dBm control to -50 dBm
- d. INTERR/SQUITTER RATE control to 270
- e. X1/X10 switch to X10
- f. SLS/ECHO LEVEL -dB to OFF
- g. POWER KW control full CCW
- h. DME PULSE P2 DEV us to 0.0
- i. VELOCITY-KTS switch to 0100 KTS
- j. DISTANCE switch to 020.00 N.M.
- k. PRF switch to 0-300 position.
- 1. SQTR switch to ON
- m. IDENT switch to OFF
- n. SYNC switch to TO
- o. DME % REPLY to 100%
- p. VAR/FREQ switch to FREQ
- q. CW switch to OFF
- r. RANGE/VELOCITY switch to RANGE
- s. Rear Panel sync switch to SYNC SQUITTER
- t. R-NAV switch to OFF
- u. TACAN SIMULATION switch to OFF
- v. LINE switch ON (red pilot lamps on)
- w. Connect cables as shown in Figure 4-4



4-19. Oscilloscope Control Settings

- a. Vertical gain control to .05 V/cm
- b. Horiz. sweep to 2 us/cm
- c. Trigger input to EXT, NEG, DC
- d. Vertical mode to CHAN. A
- e. Intensity as desired for approximately a 25 PRF trigger rate

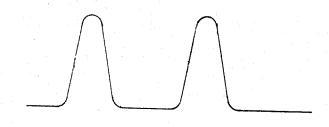
4-20. DME Control Sectings.

- a. MODE switch to OPERATE (or activate the DME for normal service)
- b. FREQUENCY switch to 108.0
- c. FUNCTION switch to 0-30 N.M. range or distance readout.

4-21. Typical DME Tests.

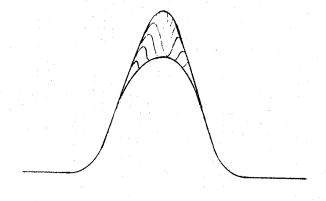
- 4-22. With all controls and cables set according to paragraphs 4-17 through 4-19, the DME should be interrogating the ATC-1200Y3 and receiving squitter at a 2700 average PRF rate and fixed range replies at 20.0 N.M. Sync to the oscilloscope will coincide with each interrogation pulse from the DME, allowing observation of the transmitter waveform. The DME should "lock on" and hold at 20.0 NM with 0 KTS velocity. Clockwise rotation of the POWER KW control will reduce the displayed amplitude of the transmitter pulses to zero (into the base line).
 - A. Transmitter Power Output. Observe the transmitter interrogation pulses to the ATC-1200Y3 as in paragraph 4-21. Slowly rotate the POWER KW control clockwise until the peak of the pulses just disappears into the display's base line. Read the peak power in KW directly from the POWER KW control scale.
 - B. Transmitter Pulse Spacing. Select the frequency specified by the manufacturer of your DME equipment for this test. Set the selected frequency on both the DME control head and the test set FREQUENCY switch. Adjust the POWER KW control for an oscilloscope display of pulses 4 to 6 cm in amplitude. Center the display vertically on the scope center graticule. The spacing from leading edge to leading edge as read on the center graticule should be 12.0us or 36.0us as shown in Figure 4-4.1.

Adjust Amplitude with Power - KW Control



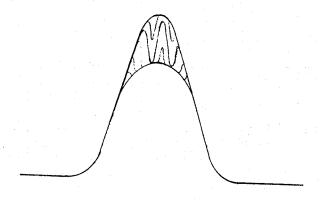
Normal DME Interrogation Pulses - X Ch.

Vert: .05 V/cm Horiz: 5 us/cm



Approximately 1
Mhz (high or low)
from center channel
frequency.

Vert: .05 V/cm Horiz: 2 us/cm



Approximately 2 Mhz (high or low) from center channel frequency.

Vert: .05 V/cm Horiz: 2 us/cm

Figure 4-6

DME Frequency Check Waveforms

- Transmitter Frequency. The DME frequency check C. function is to give rapid verification that the DME is on the proper XMTR channel to within ±1 MHz. DME sets must have an automatic standby circuit designed to allow the DME to search without receiving squitter. Refer to Figure 4-7 for the transmitter air to ground frequency for any given DME paired VOR frequency. Set the VOR frequency into the DME and select the Gz mode and the transmitter frequency on the FREQUENCY switch of the test set. Select DME FREQ CHECK on the mode switch and observe a beat pattern on the scope display. See Figures 4-6. frequency switch may be paired in 1 MHz steps to verify channel center frequency, or operated in variable mode (using a counter to read out generator frequency).
- D. Receiver Sensitivity. One method is to adjust the Output -dBm control for a very low R.F. output of -115 dBm. The DME should be in standby. Slowly increase the output level until the DME locks on. Be sure squitter is ON at a PRF of 2700 and IDENT switch is OFF. Another method is to set the Output -dBm control to a value the DME should lock on at, and change frequency throughout the band. After each new frequency is selected the DME must lock on within a short time (perhaps 2 to 5 sec). Some manufacturers also specify a reduced % reply of 70 to 80%. Adjust the DME % REPLY control for desired reply efficiency.
- E. Receiver Selectivity. Set Output -dBm control to a solid lock on value (-60 to -70 dBm), and turn IDENT switch to 1350 cycle. Set VAR/FREQ switch to VAR and monitor generator frequency with an external counter. Manually vary the generator frequency above and below the channel the DME is set to. Refer to Figure 4-7. At the high and low selectivity limits, the ident tone should stop.
- F. Decoder Selectivity. With the DME operating normally into the ATC-1200Y3, turn IDENT switch to 1350 cycle. Vary the DME PULSE P2 DEV us control plus and minus 0.5us, 3, 4, 5, and 6us. At the decoder limits called for by the manufacturer, the tone should stop.

- G. Suppressor Pulse Output. Operate the DME into the ATC-1200Y3 in RANGE mode. Sync the scope by placing the sync switch in TD, rear panel switch in SYNC SQUITTER, and observe the DECODER OUTPUT from the DME receiver. Connect a cable from suppressor output (on rear of test set) to suppr. input of DME. During the time the cable is connected approximately 30% of the squitter pulses will be dropped by the decoder.
- H. Suppressor Pulse from DME. Operate the DME in the ATC-1200Y3 in RANGE mode, and select TO sync on test set. Observe the interrogation pulses on the scope. (See paragraph 4-22a). Next observe the suppr. output from the DME on channel B of scope using ALT vertical mode. A pulse must be present with each transmitted pulse. For amplitude and width refer to maintenance manual.
- I. Pulse Repetition Frequency. Place the PRF switch in 0-300 range. Cause the DME to search by any convenient means. While in search mode, read the interrogation PRF directly from the meter. Allow the DME to lock on. Place the PRF switch in 0-30 range and again read interrogation PRF directly from the meter. Note: ATC-1200Y3 must always be in RANGE mode to use the meter to measure PRF.
- J. Auto Standby. Place SQUITTER switch to OFF. Select a frequency for the DME different from the frequency set into the test set. The DME should go into standby mode. Next change the frequency of the test set to agree with the DME frequency. The DME should still be in standby with no squitter applied. Turning on squitter should start the DME searching. Note: some lower cost DME sets will search without squitter and have no standby circuits. Consult manufacturer's manual.
- K. Range Accuracy. Operate DME into ATC-1200Y3 in RANGE mode. Set squitter to on and IDENT off. Any range set into the DISTANCE switch should be read out by the DME indicator. Check with DME specifications for values to use for calibration.
- L. Velocity Accuracy. Operate DME into ATC-1200Y3 in VELOCITY mode. Set squitter to on and IDENT off. Press SLEW switch to the right until meter indicates

desired range. Set IN/OUT switch to track inbound or outbound. Any value set into velocity switch must be duplicated by DME. Check with DME specifications for values to use for velocity calibration.

- M. Memory Time. Allow DME to lock on to test set in either VELOCITY or RANGE mode. Squitter on and IDENT off. After DME has locked on for a short time (at least 20-30 sec.) turn IDENT switch to 1350 cycle which removes the reply to the DME. After the proper memory time has elapsed the DME should lose distance readout and begin searching.
- N. Echo Detection. For the relatively newer DME's that feature echo rejection, lock the DME on to the ATC-1200Y3 in RANGE mode at a distance of approximately 40 N.M. After a solid lock on has occurred, rotate the SLS/ECHO LEVEL -dB control clockwise to ON, then slowly increase the amplitude of the ECHO pulses until the DME unlocks from its original range and locks on immediately at 30 N.M. (the fixed ECHO distance). When this occurs stop rotating the control and read in dB the relative amplitude of the echo to regular reply pulses required for the DME to sense a new reply pulse.
- O. Audio Output. Placing the IDENT switch in 1350 cycle position at any time causes a solid tone to be heard in the receiver. Audio power output, IDENT filters, etc. may be checked in this manner.

P. Other Tests

- 1. Mod. Output. The shaped DME reply pulses (and IDENT and SQUITTER) are available to modulate an I.F. signal generator or other purposes as needed.
- 2. Tacan Simulation. There are cases where a DME presents ranging or tracking problems when tuned to a TACAN (VORTAC) station, but no problems when tuned to a VOR-DME station only. The ATC-1200Y3 simulates TACAN modulation, variable from 0 to 50%, to help in spotting these difficulties.

- 3. R-NAV. Area navigation computers which accept a two pulse input from the DME for range information can be directly tested from the ATC-1200Y3. The R-NAV two-pulse output is always available whenever the set is replying to valid interrogations. Those interrogations may come from the test set itself without a DME working into it by placing the R-NAV switch to ON position.
- 4. <u>-1 Mile Switch</u>. Some models of DME equipment utilize a drum distance readout which should have a lower limit of less than 0.0 N.M. The -1 mile function allows this setting to be checked. It also subtracts one mile from any other range set into the test set as well.

4-23. USE OF ATC-1200Y3 AS A GENERAL PURPOSE GENERATOR

4-24. From time to time it may be necessary or convenient to have an L-Band, crystal-controlled signal generator around the shop. By placing the CW switch ON the ATC-1200Y3 becomes such a generator. Of course it may also be used in continuously variable frequency mode, using an external counter to determine frequency. Either way, the R.F. output is leveled, pure, and selectively attenuated for any use.

1	118 4 /		_		1						
VOR FREC (MHz)	DME RCVR GRD TO AIR		TACAN CH (SPACING)	(MHz)	DME RCVR GRD TO AIR	AIR TO GND	(SPACING)	(MHz)	DME RCVR (GRD TO AIR)	AIR TO GND	TACAN CH (SPACING)
108.00	978 1104	1041 1041	17X 17Y	112.20 112.36 112.35 112.40 112.45 112.50 112.60 112.65	1020 1146	1083 1083	59X 59Y 70Y 71X 71X 72Y 73X 74X 75X 76X 76X 77Y	116.40 116.45	1198 1072 1199 1073	1135 1135 1136 1136 1137 1137	111X 111Y 112X
108.05 108.10 108.15 108.20	979 1105	1041 1042 1042 1043 1044 1044 1045 1046 1047 1047 1048 1049 1049 1050 1051 1052 1052 1052	1771 1871 1987 1987 1987 1987 1987 1987	112.30 112.35	1146 1157 1031	1094 1094	70 X 70 Y	116.50 116.55 116.60 116.65	1199 1073	1136 1136	112Y
108.20	980 1106	1043	19X	112.40	1158 1052 1059 1053 1160 1034 1161	1095	71¥ 71¥	116.60	1200 1074 1201	1137	113X 113Y
108.25 108.30	981 1107	1044	20X	112.50	1159	1095 1096 1096	72X	116.70	1201	1138	114X
108.30 108.35 108.40	982	1044	21X	112.60	1160	1097	737	116.80	1202	1138 1139 1139 1140	114Y 115X 115Y
108.45 108.50 108.55 108.60	982 1108 983 1109	1045	22X	112.70	1161	1097 1097 1098 1098	74X	116.70 116.70 116.80 116.85 116.90 116.95	1075 12076 12076 12077	1146	116x 116Y
108,55 108,60	984	1046 1047	22 Y 23 X	112.70 112.75 112.80	1162	1099	75 x	117.00	1204	1140	117¥ 117¥
108.70	1110 985 1111	1047 1048	23Y 24X	112.85 112.90 112.95	1163	1099 1100	76 x	117.10	1204 1078 1205 1079 1206	1141 1142	118X
108.75 108.80	1111 986 1112	1048 1049	24Y 25 X	113,00	1164	1100 1101 1101	70Y 77X	117.15	1079	1142 1143 1143	118Y 119X
108.85	1112 987 1113	1049 1050	25 Y 26 X	113.05 113.10 113.15 113.20	1035 1162 1036 1163 1163 1164 1038 1165 1039 1166	1102	77Y 78X 78Y	117.25 117.30	1080 1207 1081 1208 1082	1144	119X 119Y 120X
108.90 108.95 109.00	1113 988	1050 1051	26Y 27X	113.15 113.20	1039 1166	1102 1103 1103 1104	78Y 79X	117.35 117.40	1081 1208	1144 1145 1145	120Y 121X
109.05	1114	1051 1052	27¥ 28¥	113.25 113.30	1040 1167	1103 1104	79X 79Y 80X 80Y	117.45 117.50	1082 1209	1145 1146	121Y 122X
109.15 109.20 109.25	988 1114 989 1115 990 1116	1052 1053	28Y 29Y	113.35 113.40	1041 1168	1104	81X	117.55 117.60	1209 1083 1210 1084	1146	122Y 123X
109.25	1116	1053 1054	29¥ 30¥	25 25 25 25 25 25 25 25 25 25 25 25 25 2	1040 1167 1041 1168 1042 1169	1105 1105 1106	81Y 82X	117.05 117.10 117.15 117.20 117.35 117.30 117.40 117.45 117.60 117.65 117.75 117.75	1084 1211	1147 1147 1148 1148 1148	123X 123Y 124X
109.35 109.40 109.45	991 1117 992 1118	1054	30°7	113.55	1043 1170	1106 1107	227	117.75 117.80	1211 1085 1212 1086	1148 1149	124X 124Y 125X
109.45	1118	1055	31Ÿ	113.65	1044	1107	83Y 84¥	117.85 117.90	1086 1213	1149	125Y
109.55	1119	1056	32Y	113.75	1045 1172	1108 1108 1109	83X 83X 84X 85X 85X	117.95	1213 1087 1021	1150 1150 1 084	126X 126Y 60X
109.65	994 5 1120 995 5 1121	1057	33Y	113.85	1046	1109 1110	85¥	133.35	1147	1084 1085	60Y
109.70	1121	1058	34 <u>Y</u>	113.95	1047	1110 1111	86 Ý	133.45	1148	1084 1085 1085 1086 1086	61Ŷ
109.75 109.80 109.85 109.90	996 1122	1054 1055 1055 1055 1057 1057 1058 1059 1060 1061 1062 1063 1064 1065 1066 1066 1066 1067 1068	35X 35Y	114.05	1043 1170 1174 1174 1174 1174 1174 1174 1047 1175 1070 1175 1071	1111 1112	861 X Y X Y X Y X X X X X X X X X X X X X	117.95 117.95 117.95 117.35.35 113.35	1147 1028 11483 11483 1149 1024	1086	61X 61X 62X 62X 63X
109.90 109.95 110.00	997 1123 998	1060	36 <u>Y</u>	114.10 114.20 114.25 114.30 114.35 114.40 114.45	1049	1112 1113	88 Y	11111111111111111111111111111111111111	1150	1087 1087 1088	63Y
110.05	5 1124	1061	37X 37Y	114.25	1050	1113 1114	89Ŷ	133.75	1155 11525 11525 11525 11525	1088	37447777777777777777777777777777777777
110.10	999 1125	1062 1062	38	114.35	1051	1114 1115	90¥	133.85	1026 1153	1089 10890 10990 10990 10992 100825 100825 100826	65 <u>Y</u>
110.10 110.20 110.30 110.30 110.40 110.40 110.50 110.50 110.50	1000 1126	1063 1063	39 X 39 Y	114.45	1178 1052 1179 1053 1180 1054 1181	1115	91 <u>Y</u>	133.95	1027 1154	1090	66¥
110.30	1001 1127	1064 1064	40X 40Y	114.50	1053	1116 1116	92 <u>¥</u>	134.05 134.10		1091	67¥
110.40	1002 1128	1065 1065	41X 41Y	114.55 114.60 114.65 114.70 114.75	1180 1054	1117 1117	93X 93X 94X 94X 95X	134.10 134.15 134.20	1155 1026 1150 1030	1092	687 887
110.50	1003 5 1129 0 1004 5 1130 0 1005	1066 1066	42X 42Y	114.70 114.75	1181 1055	1118 1118	94X 94Y	134.29 134.25 134.40	1156 1030	1093 1093	69 <u>¥</u>
110.60	1004	1067	43X 43X	TT4-07	1000	1119 1119	95 Y	134.45	7088	1025 1025	1 X 1 Y
110.70	1005 5 1131	1068 1068	44X 44X	114,90 114,95	1183 1057 11 8 4	1120 1120	96 x 96 y	134.50 134.55	963 1089	1026	2X 2Y
110.80	1006	1069 1069	45 X	115.00 115.05	1184 1058	1121 1121	97 <u>x</u> 97 x	134.60 134.65	964 1090 965	1027 1027	3x 3y
110.90	1007	1070 1070 1071	45X 45Y 46X 46Y	115.10	1058 1185 1059	1122 1122 1122 1123 1123	97Y 98X 98Y	134.70 134.75	965 1091	1027 1028 1028	3Y 4X 4Y
111.00	5 1133 0 1008	1071	47X	115.20	1059 1186 1060	1123 1123	99X 99Y	134.80	966 1092	1029	5x 5y 6x
111.10	5 1134 0 1009	1071 1072	47¥ 48 X 48¥	115.30	1187 1061	1124 1124	100x 100y	134.90	967 1093	1030 1030 1031	6X 6Y
111.1	5 1135 0 1010	1072 1072 1073	48¥ 49X	115.40	1188	1125 1125 1126	ioix	134.00	1093 968 1094	1031	6¥ 7x 7¥
111.2	5 1136 0 1011	1073 1074 1074	49X 49Y 50X 50Y	115.50	1189	1126	102X	135.10	969 1095	1032	8 X
111.3	5 1137 0 1012 5 1138	1074 1075	50Y 51X	115.60	1188 1062 1189 1063 1190 1064	1126 1127	1031	135.20	970 1096	1031 1032 1032 1033 1033 1034	8¥ 9X
111.4	5 1138 0 1013	1075 1075 1076 1076	51Y 52X	115.70	1191	1128	104X	135.30	971	1034	10X
111.5 111.6	5 1139 0 1014	1077	51X 51Y 52X 52Y 53X 53Y	114.995 114.905 115.001 115.015 115.235 115.235 115.25	1191 1065 1192 1066	1127 1128 1128 1129	1021	135.40	1097 972 1098	1035	ŢŢĶ
110.8 110.9 111.0 111.0 111.1 111.2 111.3 111.3 111.4 111.4 111.5 111.6 111.7	5 1140 0 1015	1077 1078 1078 1079	53Y 54X	115.85 115.90	1066 1193 1067	1129 1130 1130 1131	101X 101X 102X 103X 103X 104X 105X 105X 106X	135.50	1099	1035	12x
111.7 111.8	0 1015 5 1141 0 1016	1078 1079	54X 54Y 55X	115.95 116.00	1067 1194 1068	1130 1131	106Y	135.55 135.60	973 1099 974 1100	1035	13%
111.8	5 1142	1079 1080	55Y 56X	115.90 115.95 116.00 116.05	1068 1195	1132	107X 107Y 108X 108Y	135.65 135.70	1100 975 1101	1034 1035 1035 1036 1037 1037 1038 1039	13Y 14X
111.9	5 1143 0 1018	1080 1081	56Y	116.15 116.20 116.25	1195 1069 1196	1132	108Y 109X	05050505050505050505050505050505050505	1101 976	1038 1039	9YX 10YX 111X 112X 113X 113X 1155 1155 1155 1155 1155 115
112.0 112.0 112.1 112.1	5 1144 0 1019	1081 1082	57X 57Y 58X	116.25	1196 1070 1197	1133 1133 1134	109X 109Y 110X	135.85 135.90 135.95	976 1102 977	1039 1040	15 Y 16 X
112.1	5 1145	1082	58Y	116.30 116.35	1071	1134	110X 110Y	135.95	1103	1040	16 Y

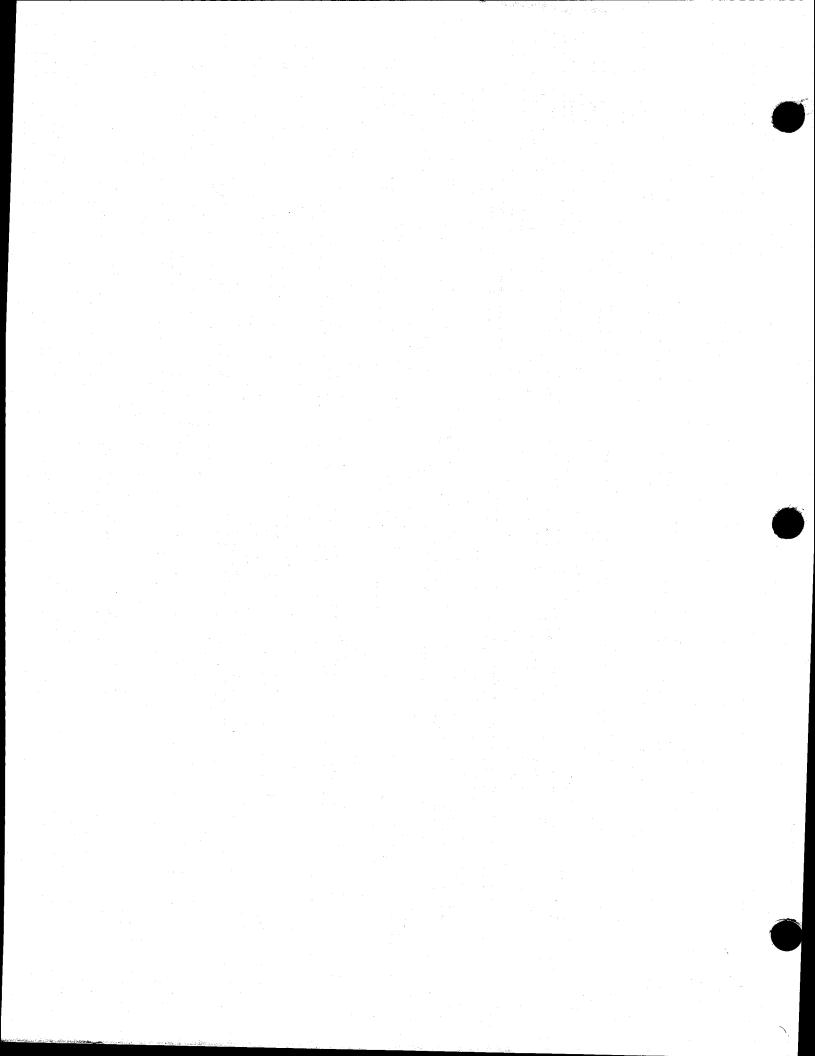


FIGURE 4-8,

DME GROUND TO AIR FREQUENCY CHANNELING

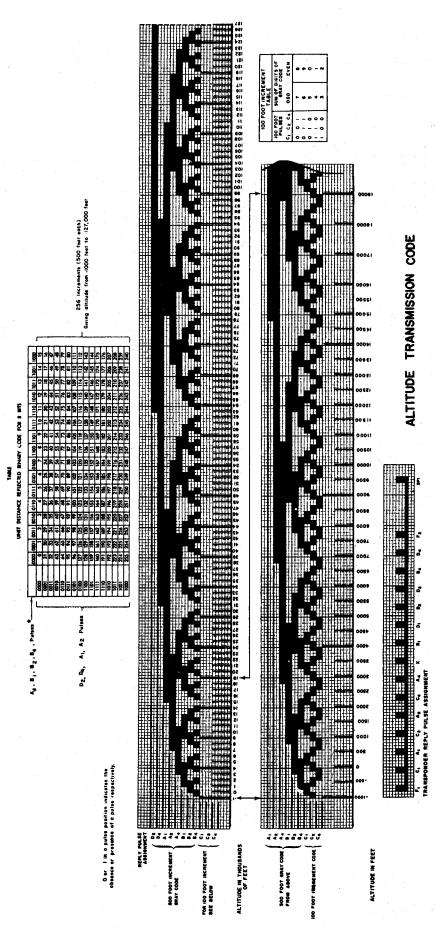


Figure 4-9 Altitude Code for Mode C Reporting

ALTITUDE TRANSMISSION CODE CHART

RANGE			ΡΊ	ULSE I	POSIT	ON					
Altitude in Thousands	D_2	D, and SPI	A ₁	A ₂	А 4	В	В2	В.,	С1	C ₂	C4
-1.0 -0.9 -0.8	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 1 1	1 1 0	0 0 0
-0.7 -0.6 -0.5 -0.4 -0.3	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
-0.2 -0.1 0.0 0.1 0.2	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
0.3 0.4 0.5 0.6 0.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
0.8 0.9 1.0 1.1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0
1.3 1.4 1.5 1.6 1.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1

RANGE				PULS	SE POS	ITION					
Altitude in Thousands	D_2	D, and SPI	A 1	A 2	Α.,	B_1	В 2	В.,	C 1	C ₂	C ₄
1.8 1.9 2.0 2.1 2.2	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
2.3 2.4 2.5 2.6 2.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
2.8 2.9 3.0 3.1 3.2	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
3.3 3.4 3.5 3.6 3.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
3.8 3.9 4.0 4.1 4.2	0 0 0 0 0	0 ° 2 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 ° 0 °	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	C O O 1 1	0 1 1 1 0	1 1 0 0 0
4.3 4.4 4.5 4.6 4.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
4.8 4.9 5.0 5.1 5.2	0 0 0 0 0	0 0 0 0 0	0 0 0 0 0	0 0 0 0	1 1 1 1	0, 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE			· · · · · · · · · · · · · · · · · · ·	PULSE	POSI	TION			,		
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂	Α ,,	В	В	В.,	C ₁	C ₂	С_
5.3 5.4 5.5 5.6 5.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
5.8 5.9 6.0 6.1 6.2	0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
6.3 6.4 6.5 6.6 6.7	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
6.8 6.9 7.0 7.1 7.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
7.3 7.4 7.5 7.6 7.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
7.8 7.9 8.0 8.1 8.2	0 0 0 0	0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE				PULSE	POSI	TION				er en	<u> </u>	
Altitude in Thousands	D	D. and SPI	A ₁	Α ₂	А.,	В1	В 2	В 4	C ₁	C ₂	С.,	7
8.3 8.4 8.5 8.6 8.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
8.8 8.9 9.0 9.1 9.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
9.3 9.4 9.5 9.6 9.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
9.8 9.9 10.0 10.1 10.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 ,0	1 1 0 0 0	
10.3 10.4 10.5 10.6 10.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 0 0 0	0 1 1 1 0	0 0 0 1 1	
10.8 10.9 11.0 11.1 11.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE				PULSE	POSI	TION						
Altitude in Thousands	D ₂	D and SPI	A ₁	A	A ,	В	В	В	C ₁	C ₂	C ₄	
11.3 11.4 11.5 11.6 11.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
11.8 11.9 12.0 12.1 12.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
12.3 12.4 12.5 12.6 12.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
12.8 12.9 13.0 13.1 13.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
13.3 13.4 13.5 13.6 13.7	0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
13.8 13.9 14.0 14.1 14.2	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE				PULSE	POSI	TION						
Altitude in Thousands	D ₂	D. and SPI	A	A ₂	A_4	В1	B ₂	В.,	C ₁	C ₂	C4	
14.3 14.4 14.5 14.6 14.7	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
14.8 14.9 15.0 15.1 15.2	0000	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
15.3 15.4 15.5 15.6 15.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 0 0 0	0 1 1 1 0	0 0 0 1 1	
15.8 15.9 16.0 16.1 16.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
16.3 16.4 16.5 16.6 16.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 0 0 0	0 1 1 1 0	0 0 0 1 1	
16.8 16.9 17.0 17.1 17.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	

RANGE				PULSE	POSI	TION					
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂	A	В	В	В,	С1	C ₂	C ₄
17.3 17.4 17.5 17.6 17.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
17.8 17.9 18.0 18.1 18.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
18.3 18.4 18.5 18.6 18.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
18.8 18.9 19.0 19.1 19.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
19.3 19.4 19.5 19.6 19.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
19.8 19.9 20.0 20.1 20.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 0 0 0

RANGE			7	PULSE	POSI	TION						
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	А 4	В	В2	В.,	C ₁	C ₂	С 4	
20.3 20.4 20.5 20.6 20.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
20.8 20.9 21.0 21.1 21.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
21.3 21.4 21.5 21.6 21.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
21.8 21.9 22.0 22.1 22.2	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
22.3 22.4 22.5 22.6 22.7	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
22.8 22.9 23.0 23.1 23.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE			J	PULSE	POSI	rion					
Altitude in Thousands	D_2	D ₄ and SPI	A	A ₂	A 4	В	В2	В	С 1	C 2	С 4
23.3 23.4 23.5 23.6 23.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
23.8 23.9 24.0 24.1 24.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
24.3 24.4 24.5 24.6 24.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 0 0 0	0 1 1 1 0	0 0 0 1 1
24.8 24.9 25.0 25.1 25.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0
25.3 25.4 25.5 25.6 25.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 0 0 0	0 1 1 1 0	0 0 0 1 1
25.8 25.9 26.0 26.1 26.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION				arthur de Allena	
Altitude in Thousands	D ₂	D ₄ and SPI	A	A2	A ₄	В ₁	В2	В,	C ₁	C ₂	С,
26.3 26.4 26.5 26.6 26.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
26.8 26.9 27.0 27.1 27.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
27.3 27.4 27.5 27.6 27.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1 1	0 0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
27.8 27.9 28.0 28.1 28.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
28.3 28.4 28.5 28.6 28.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
28.8 28.9 29.0 29.1 29.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE	PULSE POSITION										
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A ₄	В	B ₂	В	C,	C ₂	C ₄
29.3 29.4 29.5 29.6 29.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
29.8 29.9 30.0 30.1 30.2	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
30.3 30.4 30.5 30.6 30.7	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
30.8 30.9 31.0 31.1 31.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
31.3 31.4 31.5 31.6 31.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
31.8 31.9 32.0 32.1 32.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE	PULSE POSITION										
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A	В	В	В ₄	C ₁	C ₂	C 4
32.3 32.4 32.5 32.6 32.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
32.8 32.9 33.0 33.1 33.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
33.3 33.4 33.5 33.6 33.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
33.8 33.9 34.0 34.1 34.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
34.3 34.4 34.5 34.6 34.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
34.8 34.9 35.0 35.1 35.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE			I	PULSE	POSIT	rion					
Altitude in Thousands	D_2	D ₄ and SPI	A 1	A ₂	A 4	В	В2	В	C ₁	C ₂	C ₄
35.3 35.4 35.5 35.6 35.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
35.8 35.9 36.0 36.1 36.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
36.3 36.4 36.5 36.6 36.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
36.8 36.9 37.0 37.1 37.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 0 0 0
37.3 37.4 37.5 37.6 37.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
37.8 37.9 38.0 38.1 38.2	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE				PULSI	E POSI	TION						
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A 4	В ₁	В2	В,	C 1	C ₂	С,	
38.3 38.4 38.5 38.6 38.7	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
38.8 38.9 39.0 39.1 39.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
39.3 39.4 39.5 39.6 39.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
39.8 39.9 40.0 40.1 40.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
40.3 40.4 40.5 40.6 40.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
40.8 40.9 41.0 41.1 41.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	

RANGE			I	PULSE	POSI	rion			·		·
Altitude in Thousands	D ₂	D ₄ and SPI	Aı	A 2	А 4	Bı	B 2	Вч	C1	C 2	C4
41.3 41.4 41.5 41.6 41.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 0 0 0	0 1 1 1 0	0 0 0 1 1
41.8 41.9 42.0 42.1 42.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
42.3 42.4 42.5 42.6 42.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
42.8 42.9 43.0 43.1 43.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
43.3 43.4 43.5 43.6 43.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 0 0 0	0 1 1 1 0	0 0 0 1 1
43.8 43.9 44.0 44.1 44.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE	*			PULSI	E POSI	ITION						
Altitude in Thousands	$\mathrm{D_2}$	D 4 and SPI	A ₁	A ₂	A_{4}	B_1	B ₂	B ₄	C ₁	C ₂	C4	
44.3 44.4 44.5 44.6 44.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
44.8 44.9 45.0 45.1 45.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
45.3 45.4 45.5 45.6 45.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
45.8 45.9 46.0 46.1 46.2	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
46.3 46.4 46.5 46.6 46.7	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
46.8 46.9 47.0 47.1 47.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE			J	PULSE	POSI	TION						
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂	A	В	B ₂	В,	C ₁	C_2	C ₄	
47.3 47.4 47.5 47.6 47.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
47.8 47.9 48.0 48.1 48.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0	() () () () ()	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
48.3 48.4 48.5 48.6 48.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
48.8 48.9 49.0 49.1 49.2	0 0 0 0	1 1 1 1	0 0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 0 0 0	
49.3 49.4 49.5 49.6 49.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
49.8 49.9 50.0 50.1 50.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE		Taker, our was a		PULSI	E POSI	ITION						W - 112 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Altitude in Thousands	D ₂	D ₄ and SPI	A 1	A ₂	A ,,	В	В	В,	C 1	C ₂	С,	
50.3 50.4 50.5 50.6 50.7	0 0 0 0	1 1 1 1	0 0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
50.8 50.9 51.0 51.1 51.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
51.3 51.4 51.5 51.6 51.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
51.8 51.9 52.0 52.1 52.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
52.3 52.4 52.5 52.6 52.7	0 0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
52.8 52.9 53.0 53.1 53.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	

RANGE]	PULSE	POSI'	TION						-
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂	A_{\downarrow}	В	В2	B_{4}	С1	C ₂	С,	
53.3 53.4 53.5 53.6 53.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
53.8 53.9 54.0 54.1 54.2	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
54.3 54.4 54.5 54.6 54.7	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
54.8 54.9 55.0 55.1 55.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
55.3 55.4 55.5 55.6 55.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
55.8 55.9 56.0 56.1 56.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE		 ⇒ 	1	PULSE	POSI	TION					
Altitude in Thousands	D ₂	D ₄ and SPI	A 1	A ₂	A 4	В	В	В 4	C 1	C ₂	C 4
56.3 56.4 56.5 56.6 56.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
56.8 56.9 57.0 57.1 57.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
57.3 57.4 57.5 57.6 57.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
57.8 57.9 58.0 58.1 58.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1	0 1 1 1 0	1 1 0 0
58.3 58.4 58.5 58.6 58.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
58.8 58.9 59.0 59.1 59.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE			I	PULSE	POSI	ΓΙΟΝ						
Altitude in Thousands	D ₂	D and SPI	A 1	A ₂	A 4	В	В	В,	C ₁	C ₂	С 4	
59.3 59.4 59.5 59.6 59.7	0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
59.8 59.9 60.0 60.1 60.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
60.3 60.4 60.5 60.6 60.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
60.8 60.9 61.0 61.1 61.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
61.3 61.4 61.5 61.6 61.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
61.8 61.9 62.0 62.1 62.2	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	

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RANGE]	PULSE	POSI	TION					
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	$A_{\iota_{\!$	В	B ₂	Вц	C_1	C ₂	C ₄
62.3 62.4 62.5 62.6 62.7	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
62.8 62.9 63.0 63.1 63.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
63.3 63.4 63.5 63.6 63.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
63.8 63.9 64.0 64.1 64.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
64.3 64.4 64.5 64.6 64.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
64.8 64.9 65.0 65.1 65.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION				-	
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂ .	A 4	В	В	В,	C 1	C ₂	С,
65.3 65.4 65.5 65.6 65.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
65.8 65.9 66.0 66.1 66.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
66.3 66.4 66.5 66.6 66.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
66.8 66.9 67.0 67.1 67.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0
67.3 67.4 67.5 67.6 67.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
67.8 67.9 68.0 68.1 68.2	1 1 1 1	1 1 1 1	0 0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION					. <u> </u>	
Altitude in Thousands	D_2	D ₄ and SPI	A_1	A_2	A_{4}	B_1	$\mathrm{B_2}$	В _{1,}	C ₁	C ₂	C ₄	
68.3 68.4 68.5 68.6 68.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	÷
68.8 68.9 69.0 69.1 69.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	*
69.3 69.4 69.5 69.6 69.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
69.8 69.9 70.0 70.1 70.2	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
70.3 70.4 70.5 70.6 70.7	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
70.8 70.9 71.0 71.1 71.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE]	PULSE	POSI'	rion					
Altitude in Thousands	D_2	D ₄ and SPI	A ₁	A ₂	Ац	B_1	B ₂	В ₄	C ₁	C ₂	С 4
71.3 71.4 71.5 71.6 71.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 0 0	0 1 1 1 0	0 0 0 1 1
71.8 71.9 72.0 72.1 72.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
72.3 72.4 72.5 72.6 72.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
72.8 72.9 73.0 73.1 73.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
73.3 73.4 73.5 73.6 73.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
73.8 73.9 74.0 74.1 74.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION	- Anna Anna Anna Anna Anna Anna Anna Ann					Armoni con Lidia .
Altitude in Thousands	$\mathrm{D_2}$	D ₄ and SPI	A_1	A_2	\mathbf{A}_{4}	$\mathrm{B_{1}}$	B_2	В4	C ₁	C ₂	C4	
74.3 74.4 74.5 74.6 74.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1	
74.8 74.9 75.0 75.1 75.2	1 1 1 1	1 1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
75.3 75.4 75.5 75.6 75.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
75.8 75.9 76.0 76.1 76.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
76.3 76.4 76.5 76.6 76.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
76.8 76.9 77.0 77.1 77.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE			I	PULSE	POSI	rion					
Altitude in Thousands	D_2	D and SPI	A 1	A ₂	A 4	В	В2	В,	C ₁	C ₂	C ₄
77.3 77.4 77.5 77.6 77.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
77.8 77.9 78.0 78.1 78.2	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1	0 1 1 1 0	1 1 0 0 0
78.3 78.4 78.5 78.6 78.7	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
78.8 78.9 79.0 79.1 79.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
79.3 79.4 79.5 79.6 79.7	1 1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
79.8 79.9 80.0 80.1 80.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION	·					
Altitude in Thousands	D_2	D ₄ and SPI	A ₁	A2	A ,,	В	B_2	$\mathrm{B}_{\scriptscriptstyle{4}}$	C ₁	C ₂	C_{4}	
80.3 80.4 80.5 80.6 80.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
80.8 80.9 81.0 81.1 81.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
81.3 81.4 81.5 81.6 81.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
81.8 81.9 82.0 82.1 82.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
82.3 82.4 82.5 82.6 82.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
82.8 82.9 83.0 83.1 83.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE]	PULSE	POSI	TION						
Altitude in Thousands	$\mathrm{D_2}$	D ₄ and SPI	A ₁	A ₂	A 4	B ₁	B ₂	В4	C ₁	C ₂	C ₄	
83.3 83.4 83.5 83.6 83.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
83.8 83.9 84.0 84.1 84.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1	0 1 1 1 0	1 1 0 0 0	
84.3 84.4 84.5 84.6 84.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
84.8 84.9 85.0 85.1 85.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
85.3 85.4 85.5 85.6 85.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
85.8 85.9 86.0 86.1 86.2	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE				PULSI	E POSI	TION			·		
Altitude in Thousands	D ₂	D ₄ and SPI	A_1	A ₂	A_{μ}	B_1	B ₂	B_{4}	C_1	C_2	С 4
86.3 86.4 86.5 86.6 86.7	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
86.8 86.9 87.0 87.1 87.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
87.3 87.4 87.5 87.6 87.7	1 1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
87.8 87.9 88.0 88.1 88.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
88.3 88.4 88.5 88.6 88.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
88.8 88.9 89.0 89.1 89.2	1 1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE]	PULSE	POSI	TION			-		:
Áltitude in Thousands	D_2	D ₄ and SPI	A_1	A ₂	А4	B ₁	B ₂	В4	C ₁	C2	C4
89.3 89.4 89.5 89.6 89.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
89.8 89.9 90.0 90.1 90.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
90.3 90.4 90.5 90.6 90.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1
90.8 90.9 91.0 91.1 91.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
91.3 91.4 91.5 91.6 91.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
91.8 91.9 92.0 92.1 92.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION				٠.	
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A ₄	В	В2	В,	C ₁	C ₂	С,
92.3 92.4 92.5 92.6 92.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
92.8 92.9 93.0 93.1 93.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
93.3 93.4 93.5 93.6 93.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
93.8 93.9 94.0 94.1 94.2	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
94.3 94.4 94.5 94.6 94.7	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
94.8 94.9 95.0 95.1 95.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE			•	PULSE	POSI	TION					
Altitude in Thousands	D_2	D ₄ and SPI	Aı	A ₂	Ац	В1	B ₂	В4	C ₁	C ₂	С4
95.3 95.4 95.5 95.6 95.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
95.8 95.9 96.0 96.1 96.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
96.3 96.4 96.5 96.6 96.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
96.8 96.9 97.0 97.1 97.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
97.3 97.4 97.5 97.6 97.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
97.8 97.9 98.0 98.1 98.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSI	E POSI	TION						
Altitude in Thousands	D_2	D, and SPI	Aı	A ₂	A 4	B_1	B_2	В4	C ₁	C ₂	Сц	
98.3 98.4 98.5 98.6 98.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
98.8 98.9 99.0 99.1 99.2	1 1 1 1	0 0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
99.3 99.4 99.5 99.6 99.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
99.8 99.9 100.0 100.1 100.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
100.3 100.4 100.5 100.6 100.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
100.8 100.9 101.0 101.1 101.2	1 1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	

RANGE				PULSE	POSI	TION						
Altitude in Thousands	D ₂	D ₄ and SPI	A	A ₂	A 4,	В	B ₂	В,	C ₁	C ₂	C ₄	
101.3 101.4 101.5 101.6 101.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
101.8 101.9 102.0 102.1 102.2	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
102.3 102.4 102.5 102.6 102.7	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
102.8 102.9 103.0 103.1 103.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	.1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0	
103.3 103.4 103.5 103.6 103.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1	
103.8 103.9 104.0 104.1 104.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE			· · · · · · · · · · · · · · · · · · ·	PULSE	POSI	TION			,	·	
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A4	В	B ₂	В	С1	C ₂	С,
104.3 104.4 104.5 104.6 104.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
104.8 104.9 105.0 105.1 105.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
105.3 105.4 105.5 105.6 105.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
105.8 105.9 106.0 106.1 106.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
106.3 106.4 106.5 106.6 106.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
106.8 106.9 107.0 107.1 107.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE			. 1	PULSE	POSI	TION					
Altitude in Thousands	D ₂	D ₄ and SPI	A ₁	A ₂	A ₄	В	В2	В,	C ₁	C_2	С,
107.3 107.4 107.5 107.6 107.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
107.8 107.9 108.0 108.1 108.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
108.3 108.4 108.5 108.6 108.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
108.8 108.9 109.0 109.1 109.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0
109.3 109.4 109.5 109.6 109.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
109.8 109.9 110.0 110.1 110.2	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0

RANGE			1	PULSE	POS I	TION		All victories				
Altitude in Thousands	$\mathrm{D_2}$	D ₄ and SPI	A ₁	A ₂	A 4	В	B ₂	B ₄	Ci	C ₂	С,	
110.3 110.4 110.5 110.6 110.7	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 0 0 0	0 1 1 1 0	0 0 0 1 1	
110.8 110.9 111.0 111.1 111.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
111.3 111.4 111.5 111.6 111.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 0 0	0 1 1 1 0	0 0 0 1 1	
111.8 111.9 112.0 112.1 112.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	
112.3 112.4 112.5 112.6 112.7	1 1 1 1	0 0 0 0 0	0 0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1	
112.8 112.9 113.0 113.1 113.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0	

RANGE				PULSE	POSI	TION					
Altitude in Thousands	D ₂	D ₄ and SPI	$\mathtt{A}_{\mathtt{1}}$	A ₂	A_4	В	B ₂	Вц	C ₁	C ₂	C ₄
113.3 113.4 113.5 113.6 113.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
113.8 113.9 114.0 114.1 114.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0
114.3 114.4 114.5 114.6 114.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
114.8 114.9 115.0 115.1 115.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
115.3 115.4 115.5 115.6 115.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
115.8 115.9 116.0 116.1 116.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE											
Altitude in Thousands	D ₂	D ₄ and SPI	$\mathbf{A_1}$	A ₂	A	В	В	$\mathrm{B}_{_{4}}$	C 1	C ₂	С,
116.3 116.4 116.5 116.6 116.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
116.8 116.9 117.0 117.1 117.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
117.3 117.4 117.5 117.6 117.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
117.8 117.9 118.0 118.1 118.2	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
118.3 118.4 118.5 118.6 118.7	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
118.8 118.9 119.0 119.1 119.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE]	PULSE	POSI	TION					
Altitude in Thousands	D_2	D ₄ and SPI	Aı	A ₂	A4	В1	B ₂	В4	C ₁	C ₂	C4
119.3 119.4 119.5 119.6 119.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
119.8 119.9 120.0 120.1 120.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
120.3 120.4 120.5 120.6 120.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
120.8 120.9 121.0 121.1 121.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
121.3 121.4 121.5 121.6 121.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	1 1 1 1	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1
121.8 121.9 122.0 122.1 122.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE				PULSE	POSI	TION					
Altitude in Thousands	$\mathrm{D_2}$	D ₄ and SPI	A ₁	A2	A4	В1	B ₂	Вц	C ₁	C ₂	C4
122.3 122.4 122.5 122.6 122.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	0 0 0 0	1 1 0 0	0 1 1 0	0 0 0 1 1
122.8 122.9 123.0 123.1 123.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
123.3 123.4 123.5 123.6 123.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1
123.8 123.9 124.0 124.1 124.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0
124.3 124.4 124.5 124.6 124.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	0 0 0 0	1 1 0 0	0 1 1 1 0	0 0 0 1 1
124.8 124.9 125.0 125.1 125.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 0	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0

RANGE		PULSE POSITION											
Altitude in Thousands	D_2	D ₄ and SPI	A ₁	A ₂	A 4	В	В2	В,	Cı	C ₂	C ₄		
125.3 125.4 125.5 125.6 125.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	1 1 1 1	1 1 0 0	0 1 1 1 0	0 0 0 1 1		
125.8 125.9 126.0 126.1 126.2	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 1 1	0 0 0 1 1	0 1 1 1 0	1 1 0 0 0		
126.3 126.4 126.5 126.6 126.7	1 1 1 1	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	0 0 0 0	1 1 0 0 0	0 1 1 1 0	0 0 0 1 1		

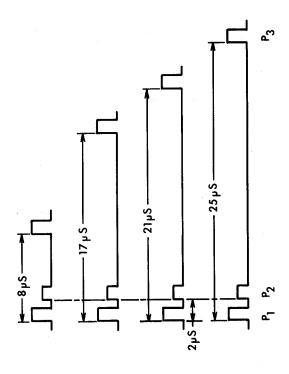
ATCRBS INTERROGATION MODES

MODE APPLICATION

3/A COMMON (ATC)

- B CIVIL (ATC) FOR U.S.
 OPERATION)
- C CIVIL (ALTITUDE)
- D CIVIL (UNASSIGNED)

CHARACTERISTIC



TRANSPONDER REPLY CODES



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PULSE NOMENCLATURE

SECTION V

Theory of Operation

- 5-1. Introduction
- 5-2. The purpose of this manual in Sections V through XIV is to give the technician all information to calibrate, repair, and prove performance of the ATC-1200Y3. This section gives specific information pertaining to theory of circuit operation, first in general, simplified terms, and second in fine detail referencing schematic diagrams.
- 5-3. General Description of Test Set Operation
- 5-4. <u>Transponder Section</u>. Refer to Figure 5-1, Simplified Video Block Diagram.
- PRF. The interrogation rate is determined by a variable PRF oscillator. The front panel Interr/Squitter Rate control and the X1/X10 switch sets the oscillator frequency from 50 Hz through 5 KHz. The oscillator is a differential controlled R-C type, temperature compensated, and is very stable.
- 5-6. The PRF oscillator output is applied to a coincidence circuit, to which is also applied the output of the CAL Mark circuitry. The coincidence circuit "stores" each PRF output pulse until the next 1.0us or 1.45us CAL pulse is applied, thus synchronizing the PRF rate and the CAL marks to present a stable scope display of both signals.
- 5-7. The coincidence circuit output is applied as the trigger to the CAL Ø one-shot, whose pulse width is controlled by the CAL Ø control. The output of this O/S will be used as the interrogation rate to the Pl-P2-P3 pulse formers. By varying the O/S time with the CAL Ø control the Pl-P2-P3 pulses can be made to vary in phase with the CAL Marks allowing precise alignment of leading edges of both pulses. The coincidence circuit output is also used as TO sync in Transponder operation providing a sync output just before Pl interrogation pulse.
 - NOTE: Using TO sync, and observing both the interrogation pulses and the CAL pulses overlaid on an oscilloscope, varying the CAL Ø control will cause the interrogation pulses to move relative to the CAL pulse which will remain stationary.

- 5-8. Interrogate Pulses. The CAL Ø O/S output (trailing edge) is applied to the Ramp Gate which turns on the Ramp Generator. The Ramp Generator output is a positive-going ramp of constant rate and amplitude with any PRF. The Ramp Gate output is also used to trigger the Suppressor Pulse O/S to form a 50us SUPPR pulse in both Transponder and DME modes. It is also used to trigger a PRF follower O/S used as the reference PRF for the squitter rate when in DME operation.
- 5-9. The start of the Ramp Generator output is the first trigger applied to an Output Pulse 0/S, and thus forms P1 of the interrogation pulses. A differential pickoff circuit samples the ramp voltage output and forms a sharp trigger pulse 2us after the start of the ramp. This is applied to the output pulse 0/S and P2 trigger pulse and forms P2 of the interrogation. A switch which is part of the SLS Level control enables the P2 Diff. Pickoff to operate only when "ON". Pickoff by the P2 DEV us control and vary the pickoff time by ±1.2us.
- 5-10. The Ramp Generator is also applied to the P3 Differential Pickoff circuit. It is similar in operation to the P2 differential except the sample voltage is variable in steps set by the Mode Switch to equal times of 8, 17, 21 and 25us after ramp start. A variable control P3 DEV us can vary each voltage step slightly to vary P3 ±1.2us from each position. The P3 Differential Pickoff forms a sharp trigger pulse applied to the Output Pulse O/S as P3 of the Interrogation pulses. P3 cannot be turned off.
- 5-11. A/C Mode interrogation is performed by having the ramp generator trigger the A/C Mode Flip-Flop to alternate set and reset position. Both sides of the flip-flop drive switches which connect precision resistors to the sample voltage side of the P3 Differential Pickoff forming alternate pickoff times of 8 and 21us on a 50-50 basis.
- 5-12. The Output Pulse O/S takes each trigger for P1, P2 and P3 pulses and makes each a pulse of nominal 0.8us. The O/S time can be varied from 0.4 to 1.2us by the Pulse Width us control.
- 5-12.1 Pre Pulse Formation. An output taken at the collector of Q809 of the CAL Ø 0/S consisting of a positive going (approximately 0.8V to 15V) pulse is applied to the Output Pulse 0/S through CR 834 with the Front Panel

- Pre Pulse toggle switch in the PRE ON position (see paragraph 3-46), the -20V reverse bias is removed from the diode CR834 This allows the positive going pulse taken from the Cal \emptyset O/S to trigger the Output Pulse O/S. The pulse thus generated is equal in width and amplitude to P1, P2, and P3, but precedes P1 by an amount of time selectable with the CAL \emptyset Front Panel control. (Approximately 2.0 to 6.0 usec).
- 5-13. The output from the Output Pulse O/S is applied to the On/Off Diode Switch Driver. The Driver applies either a full "ON" or full "OFF" voltage to the ON-OFF diode switch in the R.F. output. The CW switch when ON forces the driver to apply a steady full ON to the diode switch.
- 5-14. SLS during P2 time is accomplished by the SLS FF. The trailing edge of P1 from the ON-OFF Diode Switch Driver sets the FF which turns on the SLS Output Circuitry. The SLS Output to the RF shaping modulator is controlled by the SLS/ECHO LEVEL Control. The output can control the RF level from +1 to -10 dB relative to P1 and P3. The FF is reset by the trailing edge of P2 from the output of the Diode Switch Driver. Should this fail to reset the SLS FF, P3 differential applies a positive reset pulse each interrogation. The SLS FF does not function if P2 is turned off.
- 5-15. The output from the P3 Diff. Pickoff is used as TD Sync in Transponder Operation. On the scope display P3 will be seen at the beginning of the trace followed by the reply pulses from the transponder under test. Note that when using TD sync the transponder pulses will be stationary in the display and the CAL Marks will move in phase with variation of the CAL Ø control.
- 5-16. The CAL Marks (also called CAL Pulses) are generated by two oscillators. One is on the Phase Lock Leveler Board (located on the side of the Oscillator Attenuator Assembly) and the other is on the Transponder Board itself. The signal from the Phase Lock Board is 1.0us in period, and from the Transponder Board 1.45us in period, or spacing. The actual oscillator period on the transponder board is 0.725us, and is divided by two to achieve 1.45us. The selected CAL Mark spacing (1.0/1.45us switch) is applied to the CAL Output O/S which forms a pulse 1 V in amplitude at the CAL us Output Connector. The CAL Mark output is also applied to the Coincidence Circuit. See paragraph 5-6.

- 5-17. The Transponder % Reply FF provides a meter indication of % reply by comparing the number of interrogations to a transponder with the number of replies from it. The FF is reset by the P3 differential pickoff, which is at the end of each interrogation. It is set again by P1 of the transmitted reply from the transponder. The reply pulse is "sniffed" from the reply RF by the DME input circuitry on the DME Board. When set the % reply FF commands the meter to read 100%.
- 5-18. DME Section. Refer to Figure 5-1.
- 5-19. Decoder. The input to the DME decoder section is located on the R.F. floor directly behind the circulator in the DME Monitor Block. All incoming R.F. passes from port 1 to port 2 of the circulator and through the DME Monitor. The R.F. pulses are sniffed from a thru-line and detected by a hot-carrier diode. The output of the DME Monitor is .5 to 13 V with 10 W to 2.5 KW applied power.
- 5-20. The detected pulses are applied to the AGC circuitry where the input level of .5 to 13 V is formed to a constant pulse amplitude of 10 V P-P. This constant level allows a pick-off differential to always sample the interrogation pulses at 50% amplitude points.
- 5-21. Two other inputs are used to the AGC circuit. One is a front panel connector labeled "Test" and is used to inject a two-pulse external *generator into the test set for calibration purposes. The injected pulses should be Gaussian shaped for maximum accuracy. The other input is a self-interrogate input used to allow the ATC-1200Y3 to be used as the total DME information source during testing of R-NAV computers. The self-interrogate signal comes from the PRF Follower O/S output which is ran by the PRF circuitry on the Transponder Board.
- 5-22. The AGC output is applied to the Decoder which samples the incoming pulses at their 50% points and forms two spikes at the pickoff times. The spiker output is used for 1) a trigger to the Ranging Counter, 2) a trigger to the R-NAV Pulse Former circuit, 3) a trigger to the DME PRF O/S, 4) a trigger to the Transponder % Reply FF, and 5) a trigger to the Echo Pulse O/S. Thus when the first R.F. pulse enters the test set all DME functions are triggered simultaneously.

*DME 2-Pulse Generator IFR P/N T9-1-14-0039.

- 5-23. Within the Decoder, the first spiker output triggers an O/S. The leading edge forms TO Sync Pulse. The trailing edge starts a decoding circuit which looks for a second spike to appear either 12 or 36us after the first spike. If a valid input is sensed, the Ranging Counter output is allowed to pass to the Range O/S's and form a reply pulse pair. If no second spike is sensed, the input to the Range O/S's is held clamped to ground, and no reply is given. Whether to decode in X or Y channel (12 or 36us) in commanded by the setting of the frequency switches.
- 5-24. When using the Self-Interrogate function, only one pulse is applied to the decoder. The self-interrogate circuitry also inhibits normal decoder action to allow only one pulse to trigger all range pulse circuits.
- 8-25. Range and Velocity Circuits. The Ranging Counters are two parallel strings of 5 counters, one of which is always reset to zero unitl a trigger pulse is applied. The second counter string, if in Range mode, sets with a stored count equal to the Distance switch setting. When a trigger is applied, the first counter counts up at a rate equal to 12.359us per mile until its count is the same as that stored in the second counter. At that instant, comparators between the two counters sense the count equality. This causes, output pulse to the Sync Delay O/S. In Range mode, all Velocity circuits are gated out of the range count.
- 5-26. In Velocity mode, the Velocity Rate Synthesizer generates a frequency equal to the velocity selected by the Velocity That frequency is applied to the second range counter which counts either up (outbound) or down (in-The second counter may be fast slewed to any bound). deisred range from 0 to 300 N.N. Upon application of a trigger to the Range Counter, the first counter counts up to the count present in the second counter. Then the counter comparators give an output pulse. With each successive interrogation, the count in the second counter will be greater or lesser at a rate set by the Velocity switch. Each time the first counter counts up to that instantaneous count, the range will be greater or lesser, simulating velocity.
- 5-27. In Velocity mode, a D to A (digital to analog) converter samples the count in the second up/down counter and displays the velocity range from 0 to 300 N.M. on the front panel meter.

- 5-28. Reply Pulse Forming. The output pulse from the Ranging Counters trigger the Sync Delay O/S. Its function is to clamp squitter out of the output before a reply pulse pair is formed. A short delay of 1.5us follows the sync delay O/S initial trigger time and the output from that delay triggers the First Range O/S. When the Sync Delay O/S resets, the upward edge is used as TD Range Sync output.
- 5-29. The input to the Sync Delay O/S includes circuitry to inhibit range replies during ident periods and to drop a variable percentage of replies set by the DME % Reply control. Echo pulses also are applied at the Sync Delay O/S input and are treated as normal reply pulses. The decoder inhibit (non-valid interrogation) is applied to the Range and Echo trigger pulses at this point. When self-interrogate is activated, the decoder inhibit is prevented from operating.
- 5-30. The First Range O/S, when triggered, sets for approximately 50 or 56us depending on whether X or Y channel replies are to be formed. Its time may be shortened by 12.359us to decrease the range reply by 1 mile. (-1 Mile Switch on). When the O/S resets, the upward transition from side A triggers the Second Range O/S to set state and also sends a trigger pulse to the P1 Modulator O/S and to the Shaped Pulse O/S.
- 5-31. The P1 Modulator O/S sets for approximately 7us, during which time it turns on the On/Off Diode Switch Driver on the Transponder Board which pulls on the ON/OFF Diode Modulator in the R.F. path and applies R.F. to the Shaping Modulator (which at first is still OFF).
- 5-32. The Shaped Pulse O/S sets for approximately 4us. Side B of the O/S drives a shaping circuit which applies Gaussian DME pulses (P1 & P2) to the front panel connector Mod. Out. Side A of the O/S is a trigger pulse to the Auxiliary Circuit and operates both the R.F. Shaped Pulse Former and the R-NAV Pulse Former forming the second R-NAV pulse output.
- 5-33. During the time the Second Range O/S is set (12 or 30us), it clamps squitter from the output preventing squitter pulses between P1 and P2 reply pulses. When the O/S resets, it triggers the P2 Modulator O/S and the Shaped Pulse O/S again.

- 5-34. P2 Modulator O/S sets for approximately 7us, and similar to the P1 Modulator O/S, turns on the ON/OFF Diode Switch Driver which will apply RF to the Shaping Diode Modulator. The Shaping Modulator will be OFF at this instant.
- 5-35. The Shaped Pulse O/S sets for approximately 4us for the second time (operated first by the resetting of the First Range O/S) and again causes a shaped DME pulse (P2) to be applied to the front panel Mod. Out. connector. Side A of the O/S triggers again the R-NAV Pulse Former and the R.F. Shaped Pulse Former.
- 5-36. R-NAV. The R-NAV Pulse Former consists of a 40us 0/S which, upon setting, operates a short (7us) pulse former. Thus, when initially operated by P1, the 0/S is set and forms an R-NAV output. However, when P2 trigger is applied, the 0/S is still set from P1 and does not retrigger. The P1 to P2 reply spacing 12 or 30us will never be long enough to trigger the R-NAV 0/S a second time at P2. Therefore, only one R-NAV pulse is formed at time of initial reply pulse P1. A similar operation happens at time of interrogation when two spiker pulses are applied to the R-NAV 0/S but only the first has a trigger effect. Thus, only one R-NAV pulse is formed at time of interrogation.
- 5-37. RF Shaped Pulse Former. The Pulse Former is divided into two sections. The 3.2 μs 0/S (Q505, Q506 & associated components) sets pulse width. Output of the 0/S is sharpened by Q507 and applied to a pulse former (Q508, Q509 and associated components). Output pulse amplitude is adjusted by R530. In normal DME operation, pulse former output is switched to the shaping section of the diode switch by the echo mod board.
- 5-38.Squitter. Squitter pulses are generated on a purely random basis. A random noise generator output operates a Squitter 0/S which sets each time a noise pulse of sufficient amplitude is applied. The average rate of the Squitter O/S is controlled by a Comparator which samples the Squitter O/S output, and the output of the PRF Follower O/S. The PRF Follower O/S is operated at a steady frequency set by the PRF Oscillator on the XPDR Board. The PRF Follower 0/S pulses are rectified to for an average DC level. Squitter pulses are also rectified to for a DC level. PRF Follower and Squitter DC levels are fed to the comparator circuit which commands the Squitter O/S to slew to the desired PRF Frequency. The output of the Squitter O/S is also applied to the First Range O/S, which when set, operates the remainder of the DME pulse system to form random RF and video pulse pairs.

- 5-39. Percent Return. The Random Noise Source is also used to operate a % Return O/S on a random basis. Its output is applied to a Differential Comparator. The other comparator input is a DC level set by the % Return Control. The comparator senses both inputs and controls the trigger rate of the % Return O/S. Whenever the % Return O/S operates it inhibits all reply pulses during its set time. It does not inhibit squitter or ident pulses. When the % Return Control is at 100% the % Return O/S does not operate.
- 5-40. IDENT. The IDENT system consists of a 1350 cycle Multivibrator (MV) and a 100us Equalizing Pulse O/S which are "ORED" together to form pulse pairs 100us in spacing and 2700 total PRF rate. The MV is operated continuously when the IDENT switch is in the center or 1350 cycle position. When the MV is on all squitter and range pulses are inhibited and only ident is present at the test set output.
- 5-41. The 1350 cycle MV can also be keyed on and off by an IDENTIFIER Encoder. The Encoder is a series of R-C pulse delay amplifiers of various times. The characters of IFR (...-..) are "picked off" the Encoder by diodes and key the MV. The Encoder is recycled every 30 sec. by a 30 sec. MV. The Encoder and 30 sec MV are enabled when the IDENT switch is in IDENT ON (right) position. While the 1350 cycle MV is keyed on all squitter and range pulses are inhibited.
- PRF. When the test set is in DME RANGE mode the meter reads out the DME interrogation rate. The Spiker output from the Decoder operates a DME PRF O/S. Whenever the O/S triggers it pulls the meter toward full scale. The more the O/S operates the higher the meter reading. Two resistors that drive the meter can be chosen by the 0-30, 0-300 PRF switch to give 30 or 300 PRF full scale indications.
- 5-43. Suppressor. The Suppressor Pulse in DME Mode if formed identically to the pulse in Transponder Mode. A O/S is operated at the rate set by the PRF oscillator. Duration of the Suppressor Pulse is 50us. Note that when operating normally in DME mode the PRF control will be set to 2700 to establish an average squitter rate of 2700. This will at the same time command a suppressor rate of 2700. The suppressor PRF will be stable and squitter rate random.
- 5-44. Echo. When the ATC-1200Y3 Mode Switch is in DME mode and the SLS/ECHO LEVEL Control is ON, the spiker output from the decoder operates the Echo O/S on Pl of the interrogation. All other range reply pulse circuitry operates

normally also. The Echo O/S has a set time equal to 30 N.M. At the end of that time it resets and triggers the Echo FF to set state. The "Q" side of the Echo FF sends a trigger pulse to the input of the Sync Delay O/S which sets and starts the timing sequence as for a normal reply pulse. It also sends a pulse to the SLS Output circuit on the Transponder Board. Depending on the setting of the SLS/ECHO Level Control the Echo R.F. pulses will be varied in level from all the other output pulse pairs. When the P2 Modulator O/S resets (indicating the end of the Echo Pulse Pair time) it applies a reset pulse to the Echo FF. When the Echo FF resets it removes the command to the SLS Output circuit to alter R.F. output level. All pulses go back to the level set by the output attenuator.

- 5-45. During Echo operation all output pulses are square and not Gaussian-shaped. Turning ON the SLS/ECHO Level control removes the R.F. shaping modulation to the Shaping Diode Modulator Driver and applies a fixed DC level. Turning on the SLS/ECHO Level control also activates a circuit which decreases the time of the Pl and P2 Modulator O/S's to approximately 3.5us the 50% amplitude width of the normal reply pulse. The circuit also turns on the ECHO front panel warning lamp to notify the operator an additional reply pulse exists in the output at 30 N.M.
- 5-46. Sync. DME sync can be selected from three sources for three different displays. TO sync comes from the Decoder O/S and allows observation of 75% of the first interrogation pulse and all of the second pulse. It is used to measure power and frequency of the DME transmitter. TD sync can be selected from the Sync Delay O/S Range Sync and displays only reply pulses to the DME by the test set. Or TD can be selected from the output of Pl Modulator O/S Squitter Sync which displays all output pulses of the test set range, ident or squitter pulses. But because squitter is so prevalent over reply pulses (2700 PRF to 25 or 150 PRF) the sync is called squitter. TD sync is used primarily to observe effects of receiver pulses within the DME under test.
- 5-47. TACAN. To simulate TACAN a 60 Hz sine signal is tapped from a power transformer winding and applied to both the Shaped Pulse Output circuit and the R.F. SHAPED PULSE FORMER where it AM modulates both signals. Note that this is only a simulation of TACAN modulation and no TACAN information (bearing or heading) is present on the output signals.

- 5-48. IDENT/SELF-INTERROGATE LAMP. If the IDENT switch is set to center position or the Self-Interrogate switch is turned on, no reply pulses or many extra reply pulses are present in the output to a DME. A warning lamp on the front panel is activated in either condition to tell the operator an abnormal test condition exists. The lamp will flash in the coded characters IFR when the IDENT Switch is in the IDENT ON position.
- 5-49. XPDR/DME Switch and METER. When the ATC-1200Y3 mode switch is positioned in any Transponder mode the XPDR/DME switch (a series of switching diodes and transistors) inhibits DME modulation and applies Transponder pulse modulation to Sync Amp and applies Transponder Sync to the Sync Amp, inhibits DME shaped mod. and applies SLS mod. to the Shaping Modulator, and switches the meter to read Transponder % Return.
- 5-50. In DME mode the reverse is true. DME ON/OFF modulation from the P1-P2 Modulator O/S's is applied to the ON/OFF Diode Switch Driver and Transponder modulation is inhibited, DME shaped modulation is applied to the Shaping Diode Modulator and SLS modulation is inhibited, DME sync is applied directly to the output of the Sync Amp and Transponder sync is inhibited at the amplifier input, and the meter is switched to read DME interrogation PRF in Range operation and velocity range in Velocity operation.
- 5-51. R.F. Section. Refer to Figure 5-2
- 5-52. The L-Band RF is generated by a voltage tuned oscillator (termed VTO) in a frequency band of 950 to 1225 MHz. Output power of the VTO is approximately 300 mw. The RF output is applied to a 40 dB Isolator and then to a Distribution Block and the input of the output Attenuator. A hot carrier diode also selects the R.F. level within the Distribution Block and gives a negative output voltage proportional to R.F. power.
- 5-53. The diode output is applied to an RF Leveling Amplifier which compares the detected voltage to a reference voltage. The amplifier output is a variable voltage from 0 V to some negative value. The greater negative the level becomes the more the leveling diode, CR1101, is turned on, and greater amounts of RF can pass from the isolator to the attenuator. Bias voltage for the VTO is supplied by a bias Regulator located on the Leveler Board.

- 5-54. R.F. Output Section. The output Attenuator is a capacitive piston type operated by a 10-turn counter turning a leadscrew with 10 turns per inch. One inch of piston travel equals approximately 100 dB attenuation. The attenuator characteristics are nonlinear at settings from max. output to -30 dB, and become very linear from -30 dB to maximum attenuation available.
- 5-55. The attenuator output connector is fitted with a specially machined BNC Tee connector which applies RF power from the attenuator directly to the Diode Switch Assembly, and provides approximately 40 dB isolation from the output of a 1030 MHz oscillator to the Diode Switch Assembly.
- 5-56. The 1030 MHz oscillator output power is a nominal 5 mW and is used during XPDR or DME Freq. Check operation only. The 1030 MHz provides the interrogation signal to the Transponder at a level of -30 to -50 dB while the VTO can be operated at 1090 MHz to heterodyne with the transmitter reply pulses. The 1030 MHz oscillator is off during all other modes of transponder or DME test set operation.
- 5-57. R.F. power applied to the Diode Switch Assembly passes through two separate diode modulators. The first is used only as an ON/OFF switch and is either full "ON" or full "OFF". It is operated directly by the ON/OFF Diode Switch Driver located on the Transponder Board. When ON, it presents no more than 2 3 dB signal loss from input to output. When OFF, it has a through loss of more than 80 dB.
- 5-58. Immediately following the ON/OFF Diode Switch is the Shaping Diode Modulator. It is similar in design to the ON/OFF Switch but is driven by a variable level signal to provide a changing amount of R.F. attenuation. In XPDR modes, SLS modulation is applied to shaping section of the Diode Switch. When P2 is off, a steady dc voltage is applied. When P2 is on, the dc level from trailing edge of P1 to trailing edge of P2 may be varied to produce an attenuation range from +1 to -10 dB corresponding to SLS control dial markings.
- 5-59. In DME modes, the Shaping Modulator receives either shaped pulse information to form the Gaussian DME reply pulses or the Echo modulation (which is the same as SLS modulation) to vary the Echo pulse pair amplitude +1 to -10 dB relative to all other pulse pairs. In Echo mode, all pulse pairs are formed by the ON/OFF Diode Modulator only and are square in shape. In normal DME mode, the ON/OFF Modulator applies R.F. power to the Shaping Modulator which is controlled by the output of the RF pulse shaping circuit via the Echo Mod board.

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5-60. A note about ON/OFF Ratio: During Transponder operation, the Shaping Modulator is held ON with a loss of -1 dB continuously. Only during P2 SLS operation is the Shaping Modulator used. Therefore, the ON/OFF Ratio is established only by the ON/OFF modulator and is 80 dB or more.

In DME operation, the Shaping Modulator is held OFF except during pulse reply times so two series switches are OFF together. Their through losses add and establish an ON/OFF ratio of more than 90 dB. Note that during Echo operation, the Shaping modulator is normally ON and the ON/OFF ratio is the same as in Transponder Mode.

- 5-61. Located on the RF floor plate is a switch that selects the modulation to be used. DME Shaped Modulation comes from the RF shaped Pulse Former on the DME Board. SLS/Echo Modulation is the same modulation and comes from the Transponder Board. Echo Enable comes from the Mode Switch and switches from DME to SLS/Echo modulation when Mode Switch is set to a DME position and Echo Mod control is not set to OFF.
- 5-62. Another input is a CW switch which applies a constant ON Level to the Shaping Modulator. The CW switch also inhibits all forms of modulation applied to the ON/OFF Diode Switch Driver on the Transponder Board and pulls the ON/OFF Diode Modulator to full ON.
- 5-63. Modulated RF from the Diode Modulators is applied to the Generator Monitor where the modulation is sniffed from a thru-line by a hot-carrier diode, detected, and applied to a Video Amplifier. The Video Amplifier output is applied to the front panel "Gen Monitor" connector.
- 5-64. Intentionally omitted.
- 5-65. The RF from the Generator Monitor is applied to port 3 of circulator isolator. There it is "circulated" to port 1 and out to the external receiver. The circulator has approximately 20 dB of isolation from port 1 to port 3 when high power from a pulse transmitter is applied.

- 5-66. R.F. Input Section. R.F. Pulse energy from an external transmitter (Transponder or DME) is applied to Port 1 of the Circulator. Port 1 is the front panel Xmtr/Rec connector. Power is transferred to Port 2 and presented to the DME Monitor assembly.
- A Note About Circulators: The Circulator is a ferromagnetic device that has three operating ports through which R.F. energy transverses in both directions. It is tuned for a wide band of frequencies in our case from approx. 900 to 1250 MHz. Energy over an extremely wide power range (-120 dBm to +35 dBW) will pass from Port 1 to 2, 2 to 3, and 3 to 1 with only 0.2 dB loss. However, energy passing from Port 1 to 3, 3 to 2, or 2 to 1 will encounter approx. 20 dB or more of loss. Since the circulator depends on a strong, directed magnetic field for proper operation and low VSWR at each port, it cannot be used within one inch of a ferrous surface. Mounted within the ATC-1200Y3 the circulator spacing exceeds the min. clearance requirements.
- 5-68. The DME Monitor is a thru-line device that picks off pulse energy, detects it, and applies positive video pulses to the input to the DME Board. The pulses establish time of interrogation in DME operation and percent reply in transponder operation.
- 5-69. From the DME Monitor all R.F. pulses pass through an accurate 30 dB attenuator to reduce their power by a factor of 1000. Thus a 10 W pulse would emerge as a 10 mw pulse and a 2 KW pulse would become a 2 W pulse. This power level is applied to the Power Monitor.
- The Power Monitor acts to measure both power and fre-5-70. quency. To measure power, input RF pulses are applied to a slide-back diode, detected across it, and the video presented at the PWR Monitor front panel connector. A DC voltage is applied to the other end of the diode which when increased progressively back - biases the diode and decreases the video pulse amplitude at the power monitor At a certain voltage the video will completely disappear into the "base line" of the scope display. DC voltage level versus power input level can be accurately calibrated, and remain so over a long period of The POWER KW control supplies the DC voltage, with the knob calibrated in watts corresponding to specific voltage levels. Peak power only can be measured; however, any point on the pulse waveform can be measured for power by placing that point on the base line.

- 5-71. Transmitter frequency is measured by heterodyning the internal signal generator to the incoming RF pulses. The resultant beat frequency pattern is displayed at the Power Monitor connector. When in Freq Check Modes a diode switch located within the Counter Block Assembly directs RF energy from the VTO to a mixing diode located in the Power Monitor. The VTO frequency can be varied to determine the transmitter frequency, or the transmitter frequency can be zeroed to the VTO for on-channel adjustments.
- 5-72. Frequency Control Section. A portion of the VTO output power is directed by the Distribution Block to the Counter Block. An Isolator between the VTO and Distribution Block prevents the VTO from being phase-locked to a highpower transmitter in frequency-check operation. (Transmitter power can "back up" through the Power Monitor, through the Freq Check Diode switch and to the VTO output connector.) The Isolator also prevents the VTO from FM modulating by heavy loading caused by high-output attenuator settings. The Isolator has approximately 0.2 dB forward loss and 40 dB reverse loss.
- 5-73. In the Counter Block is a 100 MHz, crystal-controlled oscillator. The output is applied to a snap diode which generates rich harmonics of the 100 MHz input. Two Tuned Line Cavities pick off the 900 MHz harmonic and filter out all others. The 900 MHz output of the Tuned Lines is presented to a mixer diode along with the VTO output. The Mixer output will be a signal of very low level ranging from 50 MHz to 320 MHz (950 MHz 900 MHz; 1220 MHz 900 MHz).
- 5-74. A Counter Driver amplifies the Mixer output to a level capable of operating IC counters.
- 5-75. A divide-by-100 Prescaler consisting of two ÷ 2 stages and two ÷ 5 stages reduce the Mixer frequency to 0.5 MHz to 3.2 MHz. The Prescaler output is buffered and presented at the front panel CTR Output connector for external counter use, and is also applied to the frequency Switch Assembly.
- 5-76. The Frequency Switch receives the Counter Block output and further divides the frequency to achieve an output of exactly 5 kHz. The division ratio necessary to divide any input frequency (from 500 kHz to 3.2 MHz) to 5 kHz is selected by a set of thumbwheel front panel switches commanding a Programmed Divider. The switches can be set to

control the Programmed Divider in two ways: 1) in direct frequency readout of .950 to 1.220 Gz, or 2) in VOR/DME paired channel readout of 108.00 to 135.95. The switches also control the X or Y channel operation of the DME board (pulse spacings of decoder and reply circuits).

- 5-77. The 5 kHz from the Frequency Switch is applied to the Phase Lock Board for phase comparison to a reference 5 kHz. To generate the reference 5 kHz a 2 MHz crystal oscillator is divided to 1 MHz and then to 5 kHz. The 1 MHz signal is applied to the Transponder Board to use as the 1.0us CAL MARK output.
- 5-78. A Phase Comparator compares the two 5 kHz inputs and gives a DC output voltage proportional to the phase difference. That voltage is applied to one input of an operational amp. which has a reference voltage on the other input. The amplifier output goes through upper and lower voltage limit sets and is applied to the tune input of the VTO. Thus the phase lock loop is closed and total frequency control is by the Frequency Switch dividers.
- 5-79. Upper and Lower Limit Set adjustments guard against the phase comparator accidently commanding the VTO to operate out of its frequency range and having its output falling to zero. That would disable the entire loop system. Limits are normally set to 945 MHz and 1225 MHz.
- 5-80. The Phase Comparator output is checked by a Phase Monitor circuit which drives a Phase Lock Lamp as a front panel indication the phase loop is locked within narrow limits.
- 5-81. Continuously variable frequency, manually controlled operation, is obtained by breaking the phase lock loop and inserting a variable DC voltage on the VTO tune line. Two potentiometers vary the voltage in coarse and fine increments.
- Power Supply Section. The ATC-1200Y3 incorporates three power supplies yielding +20, +5, and -20 V. All supplies are electronically regulated and protected with current limiting circuits. Adjustments are provided for the +20 V and +5 V supplies. The -20 V supply is referenced to the +20 V output and is not independently adjustable.

